



amateur radio

Vol. 34, No. 9
SEPTEMBER
1966

25c

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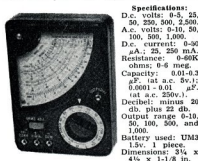
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FEDERAL COMMENT

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A.O.L.C.P. AND C.W.

At almost all recent Federal Conventions, Council has had to consider, in one form or another, the relationship of the A.O.L.C.P. holder to his request for the use and non-use of c.w. The last Convention was no exception and Council considered, and rejected, three agenda items—all variations on the same theme. Basically, this was to allow A.O.L.C.P. licensees use of all types of emission or, as a variation, the extension of operating privileges to include the 28 Mc. band. With reference to the first point, you cannot use c.w. until you have been examined and passed in it. On the second point, and at the risk of provoking some all too infrequent correspondence, it must be pointed out that whilst the Institute may appear to be unsympathetic to these appeals, International Radio Regulations preclude the abolition of the c.w. requirement below a nominated frequency.

The full text of the appropriate regulation RR41-04 of 1959 reads: "Any person operating the apparatus of an Amateur station shall have proved that he is able to send correctly by hand and to receive correctly by ear, texts in morse code signals. Administrations concerned may, however, waive this requirement in the case of stations making use exclusively of frequencies above 144 Mc." Institute representations to the Postmaster-General's Department resulted in this frequency amended to 52 Mc. You may well ask how—if there is an international regulation on the matter—can the local administration make a contrary decision? This comes about because the I.T.U. has provisions for administrations to make decisions where the results will not affect other international users. The radio isolation of Australia, in so far as 52 Mc. is concerned, was the only reason for having this frequency approved.

It should now be clear why limited licensees have no chance of getting operating privileges on the 28 Mc. band because, when in season, it is capable of providing world-wide communications.

It is interesting to note that W.I.A. proposals in 1959 advocated the reduction of the then current frequency of 1000 Mc. to 30 Mc. A compromise was reached on 144 Mc. after both the U.K. and the U.S.A. had been only in favour of reduction to 250 Mc. It would be interesting to speculate on the A.O.L.C.P. population and the present state of the u.h.f. air if the frequency had been made 250 Mc. or even remained at 1000 Mc. and the local administration had refused to agree to a reduction.

This, then, is the present situation, and whilst there are staunch supporters on both sides of the "to be or not to be" c.w. theory, the simple fact of life is that until the next I.T.U. Conference the international requirement for c.w. must stand. Whilst it is generally agreed that c.w. is a declining force in the field of communications, and could, conceivably be removed from the list of pre-requisites in the future, it still has its uses.

It is irksome and somewhat paradoxical to A.O.L.C.P. licensees to realise that whilst we are experimenting in the relatively unexplored field of space communications, and on frequencies available to the limited licensees, the only presently successful and reliable mode of communication, whether by Moonbounce or repeater satellite, is—c.w.!!

Therefore, you Z Calls, don't feel too badly about missing out on DX on 432 Mc.—after all, you can always sit for the C.W.!!

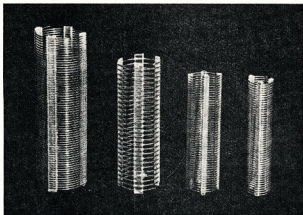
—PETER D. WILLIAMS, VK3JZ, Federal Secretary, W.I.A.

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TRANSISTOR AMPLIFIER DESIGN

R. L. HARRISON,* VK3ZRY

PART ONE

THIS article was written so that most Amateurs or other interested persons could design a transistor amplifier for low level and power r.f. and a.f. applications. Some small knowledge about transistors and simple mathematics is assumed, but the maths. is kept simple, all terms are explained and graphs are used where complicated formulae are encountered. These formulae are given though, because the graphs can only be used under certain specified circumstances as mentioned in the text.

LOW LEVEL AUDIO AMPLIFIERS

I will limit my description to a common emitter amplifier as this one finds the widest application. Fig. 1 is the circuit to which I will make constant reference.

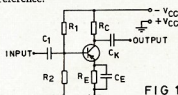


FIG 1

A PNP transistor is shown; only two things will change if an NPN transistor is used. The supply voltage V_{CC} will be reversed and the direction of the emitter arrow will be reversed. Everything else is the same (except perhaps the direction of current flow).

The first things to establish are the d.c. operating conditions. Fig. 2 will give you all the voltages and currents to be used and an explanation of the meanings of the ones that are not self-explanatory.

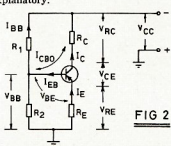


FIG 2

V_{BE} = Base to emitter voltage.

V_{CC} = Supply voltage.

V_{RC} = Voltage across collector resistor.

V_{CE} = Voltage from collector to emitter.

V_{RE} = Voltage across emitter resistor R_E .

V_{BB} = Base bias voltage.

I_{BB} = Bias components bleed current.

I_C = Collector current.

I_E = Emitter current.

I_{ES} = Emitter to base current.

I_{CBO} = Collector to emitter leakage current.

I think some explanation of V_{BE} , I_{ES} , I_{CBO} , R_E , R_1 and R_2 is necessary.

The base-emitter voltage V_{BE} is determined by I_{ES} and the internal d.c. resistance from base to emitter, of the transistor. I_{ES} is determined mainly by bias and is generally about 100 microamps. in practical circuits. The internal resistance of the transistor is about 1K to 10K ohms from base to emitter and this gives around 0.1 volt for V_{BE} . This is variable in practice, owing to changes in I_{ES} and V_{BE} and transistors, but V_{BE} is generally between 0.1 and 0.2 volt for germanium transistors. For silicon transistors V_{BE} is about 0.6 to 0.7 volt.

It will be found in practical applications that I_{ES} is around 100 to 500 μA . Now I_{ES} flows through R_2 , R_E and the base-emitter junction. From the circuit it can be seen that I_{ES} also flows through R_1 and thus I_{ES} will be a part of I_B . In a practical circuit I_B is generally between 1 mA. and 5 mA. I_{ES} is a great deal smaller than I_B and will not generally be a significant part of I_B . Thus we can assume for design purposes that I_B approximately equals I_C or—

I_B approx. equals I_C .

I_{CBO} is the collector-base leakage current, and is due mainly to minority charge carriers moving from base to collector. For germanium transistors I_{CBO} doubles its value for every 8°C. rise in temperature. Since for germanium transistors I_{CBO} is typically around 10 μA . at 25°C. (about room temperature), and will reach 0.32 mA. at 65°C., it will considerably affect I_{ES} with only a small temperature change, thus shifting the operating point. We have to design the amplifier to prevent this effect from affecting the operation of the amplifier. R_1 and R_2 are designed to minimise changes in I_{CBO} and correct these changes.

The resistor R_E is used to stabilise against forward conduction from emitter to base to ensure that I_B is relatively independent of changes in temperature. This is done to counteract the 2 mV. per °C. decrease in V_{BE} for a temperature rise.

Now that preliminary explanations and general guff are over and done with, we will get on with the design procedure (fully explained) and an example later.

(1) Choose V_{CC} . This depends on what battery or supply is convenient for you to use.

(2) Choose I_C . This is typically between 1 mA. and 5 mA. for most low level applications. If you want economy, go for 1 mA. But with silicon transistors operation is best between 2 mA. and 5 mA.

(3) Choose V_{CE} . This should be one-third or less of V_{CC} . See that V_{CE} is high enough to allow a reasonable voltage across the transistor (V_{CE}) otherwise distortion and low gain may result. Check that $V_{CE} \times I_C$ is less than

P_C max. P_C max. is typically about 0.2 watt. If $V_{CE} \times I_C$ is greater than P_C max., then lower V_{CE} to an appropriate value.

(4) Calculate R_C . The formula is as follows, if V_{CE} = one-third V_{CC} —

$$R_C = \frac{V_{CC}}{I_C}$$

This does not take into account V_{BE} which will reduce V_{CE} somewhat, but V_{CE} will decrease only a small amount (providing R_E is not too large) and this will not generally upset things.

Another way out if you know the input resistance of the following stage is to make $R_C = 5$ to 10 times R_{in} for germanium transistors and 2 to 3 times R_{in} for silicon transistors. This is because R_C is also the a.c. load (or part thereof) of the amplifier.

You can decrease R_C about half to one-third to increase the input resistance but make sure $V_{CE} \times I_C$ does not rise above P_C max.

(5) Calculate R_E by this formula:—

$$R_E = \frac{V_{CC} - (V_{RC} + V_{CE})}{I_C}$$

where $V_{RC} = I_C R_C$

Add the drop across R_E to V_{CE} , subtract this from V_{CC} and then divide by collector current. You can divide by collector current because, as explained earlier, I_C approx. equals I_B .

(6) Determine base bias resistors R_1 and R_2 . First find $V_{BE} = I_C \times R_E$, now add V_{BE} . This will give you V_{BB} .

i.e. $V_{BB} = V_{BE} + V_{RE}$

V_{BE} for normal operation of germanium transistors is 0.1 volt and for silicon transistors is about 0.7 volt. You have already found R_E , you know I_B (approx. equals I_C), so, by ohms law,

$$V_{BB} = I_C R_E$$

therefore $V_{BB} = I_C R_E + V_{BE}$.

Now determine a bleed current. Your choice will depend on economy of current (if you want it) and temperature stability. For silicon transistors I_{CBO} is extremely small until quite high temperatures are reached and the resistors R_1 and R_2 are used mainly to determine correct bias. For germanium transistors a bleed current about 20 times I_{CBO} at normal temperatures is used so that the bias will not change significantly if I_{CBO} does. For germanium transistors I_{CBO} is around 10 μA . at normally encountered temperatures, so a bleed current of 200 μA . up to 500 μA . is good practice.

Right, having chosen I_{ES} you can determine R_2 .

$$R_2 = \frac{V_{BB}}{I_{ES}}$$

$$\text{Now } R_1 = \frac{V_{CC} - V_{BB}}{I_{ES}}$$

Having calculated R_1 and R_2 , check that the ratio $R_1 \div R_2$ is less than nine (9), where $R_E = (R_1 \times R_2) \div (R_1 + R_2)$.

* 1 Mary Street, North Balwyn, E.S. Vic.

There! You have six steps, each are explained and your d.c. conditions for the amplifier should be OK.

The next thing to do is to get the thing to amplify audio signals.

Have a look at Fig. 1. There are three capacitors marked C1 (input capacitor), C_E (emitter resistor bypass) and C_K (coupling capacitor to next stage). Their values will depend on the frequency response you want.

(1) Choose the lowest frequency of interest to you. For most of you this is probably 300 cycles. Don't worry about the high frequencies yet—unless you want hi-fi. The upper frequency is determined by the transistor. If you want to cut off at 3 kc. or 5 kc. then you put capacitors across R2. More about that later.

(2) Having established your lowest frequency of interest, you give it a fancy name (censored!!). Call it the low frequency cutoff and give it the symbol f_L . The output at this frequency is supposed to be 3 db. down on the mid-range frequency (half of f_L).

If you feel mathematically energetic you can calculate C_E and C_K from the following formulae. If you don't feel so inclined then use the graphs supplied for the amplifier basic general design in Fig. 3.

$$C_K = \frac{1 \times 10^6}{2 \pi f_L (R_C + \frac{R_B R_{in}}{R_B + R_{in}})} \quad (1)$$

$$C_E = \frac{(\beta_0 + 1) \times 10^6}{2 \pi f_L (R_E + \frac{R_B R_C}{R_B + R_C})} \quad (2)$$

where C_K and C_E are in microfarads.

f_L = desired 3 db. low frequency cutoff in cycles per sec.

R_C = collector load resistor.

R_{in} = the input resistance of the following transistor (R_{in}) obtainable from the manufacturer's data but is generally in range of 300 to 1,000 ohms.

R_B = (R1 R2) ÷ (R1 + R2) or resistance of R1 and R2 in parallel of following stage.

β_0 = the low frequency, small signal current gain of the transistor (β_{DC}) obtainable from manufacturer's data. For germanium transistors it is typically 50 to 100 and for silicon transistors between 100 and 300.

π = 3.142.

From an examination of equation (1) it can be seen that C_K depends primarily on f_L and R_C. From this information and by specifying values in a typical circuit for other components we can prepare a graph of R_C versus C_K.

Fig. 3 is a typical circuit to use and small variations in R1 and R2 will not appreciably affect the graphs.

Also, from examining equation (2) we can see that C_E depends almost entirely on β_0 (or β_{DC}) and R_C, as R_{in} is relatively small under most circumstances. Two graphs for C_E have to

be plotted, one for germanium and one for silicon transistors. In the case of germanium transistors β_0 was taken as typically 50; for silicon transistors it was taken as being 150.

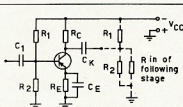


FIG 3

For this circuit:

f_L = 300 c.p.s.
R_{in} = 300, 500, 1,000 ohms (marked on graphs).
R1 = 47K ohms.
R2 = 10K ohms. (R1 and R2 of following stage).

USE OF GRAPHS

(a) Look up vertical axis (R_C) and find value of R_C you have previously calculated.

(b) Draw a horizontal line across to the appropriate curve if you know R_{in} of the following stage. If you don't know R_{in} of following stage, use curve marked R_{in} = 500 ohms for germanium transistors, or curve marked R_{in} = 1,000 ohms for silicon transistors.

(c) Where the horizontal line touches the graph drop a vertical line down to the horizontal axis (C_K or C_E) and read off value of capacitor. Use the nearest value you can buy in your circuit, or parallel an electrolytic and some disc ceramics to make a close approximation.

VALUE OF C1

By now you will be wondering what to do about C1. If this is the input capacitor to the first stage (driven by microphone, or what have you), make C1 at least as large as C_K. If this capacitor (C1) is between two stages, i.e. you have just designed the second stage of an amplifier, then find C1 as you found C_K. Use the values of R_C and R_B for the stages in use.

The usual thing to do is to design one stage and connect a couple together and then calculate the values of C_K and C_E as well as C1.

EXAMPLES

You should now be thoroughly confused—like me. Here is a worked example to clarify (or confuse?) the methods outlined above. Circuit as for Fig. 3, neglect values shown underneath.

(i) V_{CC} = 9v. I've got a 9v. battery handy.

(ii) I'm going to use an OCT1, so a collector current of 1 mA. will be all right.

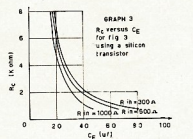
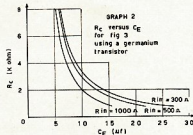
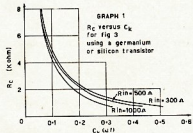
(iii) I'll let V_{CE} = 3.0 volts,
 $V_{CE} \times I_C = 3 \times 1 \times 10^{-3}$
= 3 mW.

which is well within P_C max. for an OCT1.

(iv) R_C = 3.0 ÷ (1 × 10⁻³)
= 3K ohms.

Nearest value is 3.3K ohms so I'll use that.

$$\begin{aligned} (v) R_E &= \frac{V_{CC} - (I_C R_C + V_{CE})}{I_C} \\ &= \frac{9 - (1 \times 10^{-3} \times 3.3 \times 10^3 + 3)}{1 \times 10^{-3}} \\ &= \frac{9 - (3.3 + 3)}{1 \times 10^{-3}} \\ &= \frac{9 - 6.3}{1 \times 10^{-3}} \\ &= 2.7K \text{ ohms.} \end{aligned}$$



(vi) V_{BE} = 1 × 10⁻³ × 2.7 × 10³
= 2.7 volts.

V_{BE} = 2.7 + 0.1
= 2.8 volts.

(OCT1 is a germanium transistor so that V_{BE} approx. equals 0.1 volt.)

I'll let I_{BB} = 500 μA. (0.5 mA.).

$$\begin{aligned} \text{Now } R_2 &= \frac{V_{BB}}{I_{BB}} \\ &= \frac{2.8}{0.5 \times 10^{-3}} \\ &= 5.6K \text{ ohms.} \\ \text{Now } R_1 &= \frac{V_{CC} - V_{BE}}{I_{BB}} \end{aligned}$$

$$= \frac{9 - 2.8}{0.5 \times 10^{-3}}$$

$$= 12.4\text{K ohms}$$

nearest value is 12K ohms.

Now to check the stability factor.

$$\frac{R_1 \times R_2}{R_1 + R_2}$$

$$= \frac{12 \times 5.6 \times 10^6}{(12 + 5.6) \times 10^3}$$

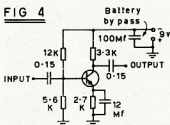
$$= \frac{67 \times 10^3}{17.6}$$

$$= \frac{3.8}{2.7}$$

$$= 1.4$$

Thus the stability is much less than nine, so the stability should be good.

FIG 4



Now we have a few resistor values:

- $R_C = 3.3\text{K ohms}$
- $R_B = 2.7\text{K ohms}$
- $R_1 = 12.0\text{K ohms}$
- $R_2 = 5.6\text{K ohms}$

and a 9v. battery is being used. All we have to do is find C_1 , C_s and C_k .

(i) The lowest frequency of interest to me is 300 c.p.s.

(ii) Seeing as $f_i = 300$ c.p.s. and I'm going to follow up this amplifier with another exactly the same, the input impedance of an OC71 will be close to 300 ohms, so I'll work out the value of C_k and C_s by using both the graphs and the formula.

From Graph 1, $C_k = 0.15 \mu\text{F}$.

By formula (1):—

$$C_k = \frac{1 \times 10^6}{2 \pi f_i \left(R_C + \frac{R_B R_{i_n}}{R_B + R_{i_n}} \right)}$$

$$\text{Now } R_B = \frac{12 \times 5.6 \times 10^3}{(12 + 5.6) \times 10^3}$$

$$= \frac{67 \times 10^3}{17.6}$$

$$= 3.8 \times 10^3$$

- Also $R_{i_n} = 300 \text{ ohms}$
- $R_C = 3.3\text{K ohms}$
- $f_i = 300 \text{ c.p.s.}$

$$\text{Now } C_k = \frac{1 \times 10^6}{2 \pi \times 300 \left(3,300 + \frac{3,800 \times 300}{3,800 + 300} \right)}$$

$$= \frac{1 \times 10^6}{2 \pi \times 300 (3,300 + 278)}$$

$$= \frac{1 \times 10^6}{2 \pi \times 300 \times 3,578}$$

$$= 0.149 \mu\text{F}.$$

Use a coupling capacitor of $0.15 \mu\text{F}$, as this value is easily obtainable. C_1 will be the same value.

From Graph 2, $C_k = 10 \mu\text{F}$.

By formula (2):—

$$C_k = \frac{(R_B + 1) 10^6}{2 \pi f_i \left(R_{i_n} + \frac{R_B R_C}{R_B + R_C} \right)}$$

- Now $R_B = 3.8 \times 10^3$
- $R_{i_n} = 300 \text{ ohms}$
- $R_C = 3.3\text{K ohms}$
- $f_i = 300 \text{ c.p.s.}$
- $R_B = 50$

$$C_k = \frac{(51) \times 10^6}{2 \pi \times 300 \left(300 + \frac{3,800 \times 3,300}{3,800 + 300} \right)}$$

$$= \frac{51 \times 10^6}{600 \times \pi (300 + 1,770)}$$

$$= \frac{51 \times 10^6}{600 \times \pi \times 2,070}$$

$$C_k = 12.8 \mu\text{F}.$$

The value of $12 \mu\text{F}$ is closer because the graphs are only correct for $R_B = 8 \times 10^3$. The discrepancy is only small in this case and a value of $10 \mu\text{F}$ in the circuit would not upset things too much.

Fig. 4 shows the completed circuit.

Now, if you want to limit the high frequency response you can put a capacitor in parallel with R_2 (base to earth) to shunt the highs.

- (i) Pick a frequency at which you want the response to drop by half (3 db.), for most Amateurs this will be 3 kc. Call this frequency f_s .
- (ii) Calculate the value of $(R_B R_{i_n}) \div (R_B + R_{i_n})$ and call it R_a .
- (iii) Calculate the value of the shunt capacitance C_s (see Fig. 5) from this equation—

$$C_s \text{ (in } \mu\text{F)} = \frac{1}{R_a} \times \frac{10^6}{2 \pi f_s}$$

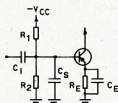


FIG 5

Example (from circuit in Fig. 4):—

- $f_s = 3,000 \text{ c.p.s.}$
- $R_B = 3.8 \times 10^3$
- $R_{i_n} = 300 \text{ ohms}$
- $R_a = \frac{3,800 \times 300}{3,800 + 300}$
- $= 278.$

$$\text{Now } C_s = \frac{10^6}{278 \times 2 \pi \times 3,000}$$

$$= \frac{10^6}{52.4 \times 10^3}$$

$$= \frac{10}{52.4}$$

$$= 0.191 \mu\text{F}.$$

Use a value of $0.2 \mu\text{F}$.

Well, that is the easy (?) way to design a low level audio amplifier without referring to equivalent circuits, hybrid parameters and a mass of manufacturer's data. I suppose it seems a bit long but once you've tried it, it becomes quite easy. A second article (Part Two) will give you an easy method of designing low level r.f. and i.f. amplifiers. A third article will deal with power r.f. and a.f. amplifiers.

REFERENCES

- (a) "Transistors," by Milton S. Kiver.
- (b) "Reference Manual of Transistor Circuits," by Mullard.
- (c) "73" Magazine, January 1965.
- (d) "Electronic Fundamentals and Applications," by John D. Ryder.

FURTHER NOTES ON VK4AT's POWER SUPPLIES

Quite recently I acquired a power supply with two different circuits attached, a 500-volt a side h.t. supply and a 75-volt a side bias supply.

This latter I wished to alter to an orthodox supply for my v.f.o.

Now under the original wiring scheme the common wires of each circuit were the common common wires. Therefore the correctly marked terminals were the common common common designated terminals. However, when changing one of the systems as above I quite naturally assumed that the common wires of the circuits were common common wires and I attached them accordingly.

Barrie VK4LN nearly had a fit at the sight of it. He explained that, under the changed system I had a common designated terminal that was now a centre tap and thus to be grounded. This didn't alter the fact that its wiring was still common, common only to that particular circuit. It was not common to the common common wires of the circuit as a whole. The wiring in the other circuit would now be common common wires only until it had ceased to be common to both common designated terminals.

This severance had become necessary now because of the potential difference between the two common systems.

He must have been right as the power supply now works as intended.

It appears that a common common is only feasible in a multiple circuit, with the common common common to each common circuit, and thus with no potential differences in any section of the common wiring.

As you could not differentiate in the term at any point, you must have a common common in each leg.

Under these circumstances would it be a common common or a common common to both circuits?

—A. J. C. Thompson, VK4AT, Skyring Creek, Pomona, Qld.

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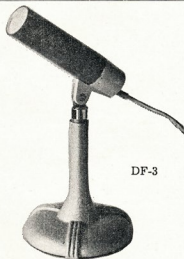
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SIDE BAND

Sub-Editor: PHIL WILLIAMS, VK5NN

During the past year or so I have been asked many times how to operate the old a.m. transmitter final as a linear amplifier for s.s.b. My answer is that in many cases the additional power which can be obtained with the existing power supplies, is not worth the extra trouble if the existing exciter uses a pair of 6146's or similar t.v. line tetrodes in class AB1. Since there are some exciters which use small tubes giving approximately 20 watts of power, the question of pressing the old 813 or similar final into use, arises.

distortion products and their owners are "warned off" by the neighbouring Amateurs.

One satisfactory circuit, which supplies r.f. drive to the zero-biased grid, and rectified "s.s.b. envelope" to the screen grid, is the "G2DAF Linear Amplifier," developed and patented in England by G. R. B. Thornley. The circuit is shown in Fig. 1.

Salient points worthy of mention are the necessity for swamping the input by a 500 ohm resistor for the benefit of the driver stage and the 27K bleeder across the screen grid by-

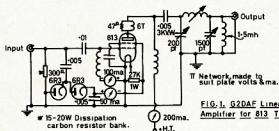


FIG. 1. G2DAF Linear Amplifier for 813 Tubes.

To use these large tetrodes in class AB1 requires reasonably high bias (90v.) and screen grid voltage (600v.) and with low anode volts such as used in the old a.m. rig (say 1000 volts), the plate efficiency is low, the screen current may be high, the plate current under speech conditions without flattening is disappointingly low, and the complete exercise is hardly worth while—particularly after the neutralising operation. The only saving feature is the low drive requirements. Better results may be obtained by class AB2 operation with about 350 to 400 volts in the screen grid, but the grid circuit must be operated with "high-C" and some swamping resistance (about 2000 ohms) to minimise distortion. A stiff bias supply is essential.

The elimination of screen grid and bias supplies can save complication and has been responsible for Eimac's triodes such as the 3-400Z being designed for zero bias operation in the grounded-grid mode. Such tubes are expensive but give low distortion in relatively simple circuits.

Several circuits which were developed 7 or 8 years ago used gated screen supplies for the 813 amplifiers, viz., the ZL-Linear, and the G2MA linear amplifier. These have worked well for those who are satisfied to operate them at very low plate current, but most people have been accustomed to more than 70 to 80 mA. in an 813—one may as well use an 807 and save the 50 watts of filament power. When pushed any harder than this, these amplifiers emit excessive

pass capacitor. Some 813's do not appear to need it, but for older tubes it has been necessary to return the screen voltage to zero between words and syllables. The diodes recommended for the Cockcroft-Walton voltage doubler for the screen supply are 6V. booster diodes, with high heater-cathode voltage rating 6R3's or 6AL3's should be adequate. The 813 should not be driven beyond 150 mA. on single-tone input which requires about 20 watts of drive. Plate circuit tuning component values will be determined by the plate voltage used, but the amplifier is efficient as the peak screen voltage is only about 105 volts.

The amplifier was described in the "R.S.G.B. Bulletin" for April, 1963, page 518. Further correspondence is to be found in the September, 1963, issue on page 199 and October, 1963, on page 231. Although I have not used this circuit, reports from users in England and Australia indicate that, when correctly loaded, the amplifier is capable of good output with low distortion. Reports of t.v.i. in the London area were traced to the higher output from the transmitter and the fact that B.B.C. television is on the third harmonic of the 14 Mcs. band. A 7094 amplifier in class AB1 was shown to produce similar interference under the same conditions.

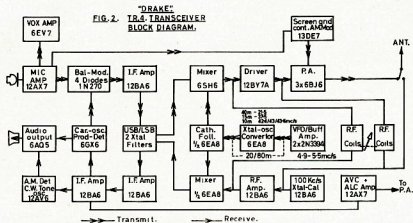
THE DRAKE TR-4 TRANSCEIVER

By courtesy of Arie VK2AVA we have, this month, a run-down on this unit which is a very nice little job, now very popular in the U.S.A., but there are relatively few of these in VK at the moment.

"The Drake TR-4 s.s.b./a.m./c.w. transceiver is the most versatile unit in its class presently on the American market. It is the only one providing also near a.m. output, has v.o.x. control, break-in c.w. u.s.b./l.s.b. selection and crystal calibrator as standard equipment. It also has a true a.m. envelope detector on reception. Size 5½ in. x 10½ in. x 14½ in. deep, weight 16 lb., 300w. peak input, power requirements 650v. at 300 mA., 250v. at 175 mA., 45-65v. bias and 12.6v. a.c./d.c. at 5.5a. Nominal output 50 ohms resistive. It uses 20 tubes (1 regulator), 9 diodes and 2 transistors (v.f.o.).

"It follows the now almost common practice of a fixed tuning range for the v.f.o. of 4.9-5.5 Mc. and crystal-controlled pre-mixing before the resultant heterodyne range is mixed with the incoming or outgoing signals. For instance, on 15 mx the v.f.o. signal is subtracted from a 35.5 Mc. crystal signal, giving a heterodyne range of 30.6-30.0 Mc., resulting in a 21.6-21.0 Mc. range after subtraction of the 9.0 Mc. crystal filter i.f. frequency. This system has the advantage of better stability in the v.f.o., better calibration, no v.f.o. switching. Also there is a higher image rejection

(Continued on Page 11)



THE 80 AND 40 METRE "TRANSISTOR SPECIAL"*

JOHN S. HILL. K4OJZ

MOST Amateurs consider transistors beyond their pocket book and technical ability. Actually they can be less expensive and easier to handle than vacuum tubes. The rig described was built for a Novice nephew. It is also an ideal Field Day or brief-case transmitter for the James Bond set. Unlike so many transistor transmitters it has sufficient output to deliver a healthy signal and weekly schedules have been maintained in the Novice bands over a 600-mile distance.

CIRCUIT DESCRIPTION

A transistor equivalent of the Pierce oscillator is used. Any crystals including low drive surplus metal can units can be used. 40 metre operation with 80 metre crystals is possible with some output decrease.



Top view of the transistorised 80-40 metre Novice c.w. transmitter. All controls are clearly marked. Note how the crackle finish was neatly removed in the area of the two output transistors for more efficient surface contact.

The oscillator is followed by an emitter tube cathode follower. Since the oscillator is relatively high impedance and the input impedance of the p.a. is very low, either tuned circuits or an impedance matching stage must be used. Power gain is limited with transistors at high power levels and the buffer gives about 10 db. gain which permits the oscillator to operate at low power. The original unit built did not include a buffer and worked well but the high oscillator input, about 1 watt, produced severe chirp and crystal drift.

The power amplifier uses two transistors to deliver about 16 watts output on 80 and 11 watts on 40 metres with a 24-26 volt power source. Input is 20-15 watts. Operation at 12-15 volts is possible but output will be about 5 watts on 80 and 0.25 watt on 40.

The power amplifier output impedance is very low, about 26 ohms at 12 watts output. An L-pi output circuit gives reasonable component values, excellent harmonic suppression, easy duplication and ease of tuning plus transistor protection. The L section (L1 and part of the tuning capacitor) transforms the low collector impedance to several thousand ohms where a conventional "vacuum tube" pi section can be used for tuning and loading. A

- This compact (2" x 3" x 5") 40 and 80 metre transmitter is completely transistorised, simple to construct, low cost, will operate into any antenna and produces 15 watts or more output.

switch is used to add tuning capacitance for 80 metres and the combination of a fixed and variable loading capacitor permit any antenna over 10 feet to be used on either band. Bulb type p.a. current and antenna voltage/current indicators are used for easy tuning, size, and cost reduction.

A d.p.d.t. switch is included for transmit-receive. In the receive mode the oscillator and buffer can be keyed

TUNING

No tuning other than the final is required. Unlike vacuum tube transmitters, the p.a. draws very little current until fully loaded whether off resonance or not. The L network is basically a high impedance at all frequencies other than resonance, the opposite of a conventional parallel tuned vacuum tube tank circuit.

Transmitter adjustments should always be for **maximum output**, not minimum p.a. current. P.a. current measurement is included only to indicate relative power input. Adjust p.a. tuning for maximum output (antenna current) voltage indicators then adjust p.a. load for higher output if possible. Continue adjusting both until no further output increase is noted. With a 50 ohm load, typical total capacitor values are:

| | | |
|------|-----------|-----------|
| | 80 Metres | 40 Metres |
| Tune | 390 pF. | 105 pF. |
| Load | 500 pF. | 310 pF. |

If antennae under 30 feet or half-wave are used, the output capacitance will be much less and the tuning capacitance more; the No. 49 bulb will show less current, but the neon bulb will ignite showing high voltage feed. In general, tune for maximum antenna bulb brightness regardless of load.

A calibrated wavemeter or S meter should be used for initial tune-up on 80 metres since the final doubles very efficiently. Mark the capacitor settings for future reference.

COMPONENTS

The chassis used was a BUD, CU 3006A. The PADT 50's are mounted on one end using the entire case as a heat sink. Clean off the crackle finish, use mica insulating washers and a silicon grease when mounting. RFC1 should be low resistance; use a 1" loop stick core and at least 20 turns of No. 28 wire or larger. No component values

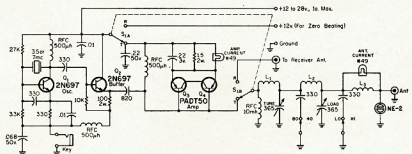


Fig. 1.—Circuit of a transistorised 80 and 40 metre c.w. transmitter. The buffer heat sink must be in 10 in.² and the Power Amp. heat sink 29 in.². All capacitors greater than one are in pF.; those less than one are in μ F. All resistors are $\frac{1}{2}$ watt unless otherwise noted. Currents shown are for a 25 volt supply on 80 metres with 16 watts output.

- L1-22 turns $\frac{3}{4}$ inch o.d. at 32 t.p.i. Air Dux
632 or equiv.
L2-30 turns $\frac{3}{4}$ inch o.d. at 32 t.p.i. Air Dux
632 or equiv.
L3-5 turns cotton covered wire on small $\frac{3}{4}$
inch powdered iron core.

Adjust turns for normal lamp brightness at maximum output into 52 ohm load.

RFCI—See text.

* Reprinted from "CQ," April 1968.

are critical except for the p.a. coils which should be close to the values shown.

The NE-2 antenna voltage indicator should be mounted flat against the chassis near the No. 49 bulb with both leads connected to the antenna lead and only stray capacitance to ground. To save money the indicator bulbs may be mounted by pushing them through a rubber grommet.

The oscillator transistor requires no heat sink. The buffer transistor runs hot and a good heat sink must be used.

The overall size of the transmitter can be greatly reduced by using mica compression trimmers, Arco No. 303, for tuning but special knobs or screw-driver adjustments are required.

OTHER BANDS

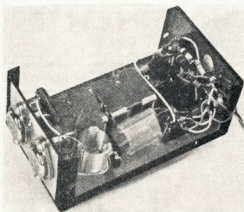
No changes are required for operation on any frequency from 3-8 Mc. Operation on 160 metres at full power can be obtained by changing L1 and

L2. Twenty metre or higher operation is not practical except at very low output, about 4 watts on 20, and 2 watts on 15, using half frequency crystals. Inductors L1 and L2 have to be changed for either band.

RESULTS

The first two contacts using a dipole were a VE3 on 80 and a W7 on 40. Both answered CQs on a Saturday night on the first call! Neither realised that low power was being used, much less transistors, until told so, at which point I suddenly became 599 instead of 579.

Since that time schedules have been maintained on a regular basis day and night from Connecticut to North Carolina with a Novice using a "disguised antenna" (fine magnet wire any length thrown into the nearest tree with no insulators). The power supply is two small 12 volt Ni-Cad batteries and a trickle charger.



Overall view of the interior of the 20-40 metre Novice transmitter shows the location of the loading and tuning capacitors and the coils. The buffer and oscillator circuits are on the right end of the chassis.

SIDEBAND

(Continued from Page 9)

or suppression as unwanted mixing products fall far outside the wanted range.

The double 9.0 Mc. crystal filter is a luxury, the job could have been done with one filter and u.s.b./l.s.b. carrier crystal switching. However, as the carrier crystal frequency remains constant, there is never any chance of operating frequency shift when changing sidebands. The a.m. operation, with a diode detector and no b.f.o. interference on reception, is unique. Full carrier is inserted by unbalancing the balanced modulator and the screen supply to the final tubes passes through the low-mu triode section of the 13DE7 audio-amplifier, giving a type of controlled carrier amplitude modulation, not unlike s.s.b. operation. The final stage can therefore handle a fair amount of a.m. as no constant carrier limits the input to the final.

The set is provided with a plug for external second v.f.o. operation. With

the proper extra v.f.o. unit connected, switching of the particular wanted v.f.o. on reception or transmission is done automatically through the internal transmit-receive relay and controlled by a 4-position knob on the external v.f.o. One can then transmit and receive on two different frequencies in one band. Some tricky switching and input-output coupling to the filter is used, but otherwise the circuits follow normal s.s.b. design practice. Note in the block diagram that the final amplifier output stage is separated from the receiver tuned circuits. They are paralleled with other high impedance tuned circuits in the transmitter line-up providing better selectivity.

"The Drake TR-4 is a well-built unit with a well-calibrated dial and linear permeability tuning over the full v.f.o. range. It has a good receiver but its a.v.c. action and S-meter operation leave a bit to be desired. One has to 'fiddle' with the r.f. gain control to keep strong signals from distorting. The lack of an audio amplifier between the product detector and audio out-

put stage no doubt makes the detector do overtime! Also, there is a "birdie" on reception on 21.2 Mc., the fourth harmonic of the v.f.o., and on 40 metres strong signals will show up on odd spots. The cause of this is that the third harmonic of the v.f.o. overlaps the heterodyne mixing range in the 16 Mc. range. However, these odd signals are 60 db. or so down on the unwanted spots, so never very loud and they tune three times faster than the genuine signals. It would have been better if the 40 metre band coverage had been 6.7-7.3 Mc. A change in the conversion crystal of 21.5 to 21.3 Mc. would do the trick as the odd reception signals would then fall outside the Amateur band range (below 7.0 Mc.)."

Correspondence received has included many requests for information on equipment. I gather there are many Amateurs who do not have access to overseas literature and so do not have much of an appreciation of the commercial type numbers and what they represent. One Amateur said he did not want these descriptions so that he could buy the gear but so that he would not have to sound so ignorant while in QSO with overseas stations. This point of view is appreciated, and Arie has promised further information which should help to satisfy the demand for information. 73, Phil SNN.

TECHNICAL ARTICLES

Readers are requested to submit articles for publication in "A.R." in particular constructional articles, photographs of stations and gear, together with articles suitable for beginners, are required.

HINTS AND KINKS

FILED INFORMATION

The following is an idea which I feel may be of interest to many Amateurs who, like myself, often have difficulty in remembering details of past QSOs, names, places, whether QSLs have been sent or received, etc., etc.

Simply it involves printing a QSL card which consists of two parts. One is the normal card giving details of the QSO on the standard QSL size of 5 1/2 x 3 1/2.

The other section, which can be any desired size, is a tear off section on which details of the QSO can be recorded and filed for future reference when required.

Thus in one simple operation a QSL can be written and details filed. I feel sure that the little extra cost involved in printing would be well repaid.

Geoff Wilson, VK3AMK.





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| Frequency response | | 200 to 10,000 c.p.s. |

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AN F.E.T. PREAMP. FOR 144 Mc.*

ALLEN KATZ, K2UYH

ALTHOUGH transistorised pre-amplifiers have been on the v.h.f. scene for several years, they have never really found acceptance on the 2 metre band. On the other hand, transistors are in almost universal use on the 70 Cm. band. The reason for this neglect on the part of two metre operators is twofold. First of all there is the feeling that nothing can beat the performance of the vacuum tubes presently in use. And secondly, there is the knowledge that transistors do tend to overload much more readily than tubes.

Possibly if more two metre operators were aware of the fantastically low noise levels transistors now produce on 432 Mc. they might begin to question the perfection of their tube front ends. (It is now possible using the best in low noise v.h.f. transistors and common emitter circuits to obtain a noise figure on 432 better than that of a 416-B on 144 Mc.) But then again there is still the problem of overload and cross modulation. After all how many 70 Cm. stations have to put up with the equivalent of a fellow with a Gonset a few blocks away. It is this problem of overload which first brought the f.e.t. to our attention.

names of the f.e.t. elements which correspond respectively to the grid, cathode and plate of a vacuum tube. As expected, the P channel biases exactly opposite to the N channel type.

The noise figure of a good v.h.f. f.e.t. remains almost constant (approximately 1.5 db.) as frequency is increased up to about 200 Mc. and then rises sharply. Thus, though an f.e.t. at the present stage of the art will not produce as good a noise figure as that of many transistors on 432 Mc. (about 4 db. minimum), it should perform as well or better than the best transistor on 144 Mc.

It is said that the proof of the pudding is in the eating . . . and there is no better proof than hearing with one front end that which you can not hear with another. When we constructed our first f.e.t. pre-amp. we did not expect to hear anything outstanding. For how much better can one get than a good 416-B on two metres? Maybe one db. On this point we were greatly astounded. For after the initial tune up, we found that we could pull signals which were undetectable on the 416-B about half an S unit out of the noise with the f.e.t. To say the least we were jubilant. Furthermore, the f.e.t. performed as predicted and gave us no trouble with overloading.

CIRCUIT

Fig. 1 shows the schematic of a 144 Mc. pre-amp. using an N channel (TI 2N3823) f.e.t. in a common source circuit. F.e.t.s may also be used in common gate configurations (the f.e.t. equivalent of grounded grid), but common source appears to give a better noise figure.

The circuit is simple and the components inexpensive. Thirty-five cent 1-10 pF. tubular plastic piston trimmers are used to tune the input and output circuits to resonance. The tap on the input coil should be adjusted for best noise figure, which according to theory is about one-eighth of the way up the coil from the grounded end for a 50 ohm input. We found the optimum tap point to be closer to one-quarter of the way up. The output coupling loop is adjusted for maximum gain. Bias is provided by a 3.9K source resistor which should supply about -2.5 volts of gate bias for a 9 volt drain supply.

CONSTRUCTION

The amplifier was constructed on a 4" x 24" piece of copper clad board. Ordinary copper or brass plates could be used as well; we just find printed circuit board a particularly easy material to work with. The photograph and Fig. 3 show the layout. Care should be taken to make sure the input and output circuits are well shielded from each other. If this precaution is not followed a neutralisation problem may

develop. In the two f.e.t. pre-amps. we have constructed thus far no such problem was encountered. However, should neutralisation prove a problem, inductive neutralisation, as used in vacuum tube circuits, may be used to cure it.

The amplifier described in this article is now in use at WA2FGK's QTH. Andy's operating results using the amplifier speak for themselves.

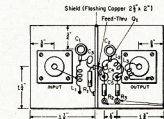


Fig. 2—Layout of the f.e.t. two metre pre-amp. built on a 4 x 2 1/2 inch copper clad board. The shield is a 2 1/2 x 2 inch piece of flashing copper.

One final note, remember that an f.e.t. pre-amp. will add about 12 db. of gain to your receiving system. Thus though the f.e.t. front end may not overload, this does not mean that your h.f. receiver's front end will not overload. To avoid this problem, insert a variable pad between your converter and h.f. receiver. Adjust the attenuation of the pad to a point where the noise output of the converter just rides over the noise level of your receiver. ●

* Gienzer, K., "T-Pads for R.F. Circuits," "CQ," July 1964, p. 31.

★

"THEY AND ME"

Ever hear a member say—"THEY ought to run our club this way?"
Ever wonder who are THEY, who get the brunt the live-long day?
THEY are the ones some call a clique, who plan the work and make things tick.
THEY fix the lights and sweep the floor; THEY handle every needed chore.
THEY keep the clubroom up to snuff; THEY worry about the heat and stuff.
THEY line up speakers, pictures too, and the people who will work for you.
THEY do the leg work, write the mail, provide a programme without fail.
Directors' meetings THEY attend, committee meetings without end.
On evenings THEY could spend at home, on your club's business THEY must roam.
THEY take new members into hand; THEY run instruction sessions, and . . .
THEY must manage all the work other members prefer to shirk.
Some pay their dues and think they may stand and smirk.
THEY pay the same dues, it's true, but gain no more than YOU and YOU.
Is paying dues your duty's end, or can a helping hand you lend?
As true as "GOD can make a tree," YOU ought to change the THEY to WE.

—"Scars News."

Fig. 1—Circuit diagram of the two metre f.e.t. pre-amp. All capacitors are in pF. and all resistors are 1/2 watt.

FIELD EFFECT TRANSISTORS

The f.e.t., a relatively old semiconductor device (first patented in 1935), has only recently become available to the Amateur and the electronics industry in general. Its operation, covered in several good articles, resembles more closely that of a pentode vacuum tube than any transistor. It has a high input impedance as contrasted to the low input impedance of a regular transistor. It is this quality which explains the f.e.t.'s high resistance to overload and cross modulation, and our interest in the device for use as a two metre pre-amp.

There are two types of f.e.t.s (N channel and P channel). The N channel biases identically with the triode vacuum tube (negative voltage on the gate, positive voltage on the drain). The gate, source, and drain are the

* Reprinted from "CQ," May 1966.
* Brown et al., "V.h.f. Column," "CQ," Nov. 1965, p. 62.
* Kolk, P., "The Insulated Gate F.E.T.," Kmc. Semiconductor Corp., Long Valley, N.J., Nov. 1964.
* Angelo, E., "Electronic Circuits," Second Edition, 1964, McGraw Hill, p. 210-211.

* Application Notes, "V.h.f. Tuned Amplifiers Using the TI 2N3823 F.E.T.," Texas Instruments Inc., Dallas, Texas, Sept. 1965.

SUNSPOTS AND PREDICTIONS

Frank Hine, VK2QL, has agreed to prepare an article for "A.R." on the aspect of propagation as it specifically applies to the Amateur Service and will include discussion on the Prediction Charts as supplied by I.P.S. and currently appearing in "A.R."

In the meantime, the following tables are the mean and smoothed mean sunspot numbers which he receives from I.P.S. This covers from the minimum period in 1954, and any Amateur taking the trouble to analyse the table will see that the increase in sunspot numbers of the current cycle is greatly lagging the peak of the record-breaking cycle and the climb to that peak.

Briefly, the "mean" indicates the average number of sunspots observed during a particular month, and "smoothed mean" is a 12-month running period of observation. It is the smoothed sunspot number, plotted over a long period of time, which exhibits the well known cycle variation.

The Observatory at Zurich, which has maintained records since 1749, has estimated the next peak in 1968.7 will reach only 100 as against the last peak of 201.2 in 1958.

Pending information to be supplied in greater detail, users of the charts may find the following of assistance.

The M.U.F. curve is the Maximum Usable Frequency for reliable communication by means of F layer reflection. Above that frequency, reflection may not be expected.

The A.L.F. curve is the Absorption Limiting Frequency, or the lowest useable frequency predicted, and frequencies below that can be expected to be absorbed beyond the ground wave. However, the closer we get to the A.L.F. the greater the absorption and the weaker the signal.

Where the A.L.F. curve crosses and exceeds the M.U.F. curve in frequency, no communication is possible by F layer reflection.

Do not take the times shown in Al VK4SS' DX column as factual for VK. He is dependent, as I was, on overseas

information for his column. The times are often suitable for the opposite hemisphere, as for example, the reference to TN8AF in July "A.R." The short path to West Africa M.U.F. is only 11 Mc. at 2000z, whilst on the long path the A.L.F. exceeds 14 Mc. For VE1AED in Egypt, the A.L.F. exceeds

14 Mc. from 0430z to 1100z, so you see you would be wasting your time if you expected to hear those stations under normal propagation. I say under normal, but keen DXers know that without warning, we get abnormal conditions when anything can happen—VK2QL.

COMPLETE SUMMARY OF SMOOTHED MONTHLY MEAN VALUES OF SUNSPOT NUMBERS AT ZURICH

| Year | Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sep. | Oct. | Nov. | Dec. |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1954 | 6.4 | 5.6 | 4.2 | 3.4 | 3.7 | 4.2 | 5.4 | 7.2 | 7.8 | 7.9 | 9.4 | 12.0 |
| 1955 | 14.2 | 16.4 | 19.5 | 23.4 | 28.8 | 35.1 | 40.1 | 46.5 | 55.5 | 64.4 | 73.0 | 81.0 |
| 1956 | 88.8 | 98.4 | 109.2 | 118.8 | 127.4 | 136.9 | 145.5 | 149.6 | 151.4 | 156.0 | 159.9 | 164.3 |
| 1957 | 170.2 | 172.2 | 174.3 | 181.0 | 185.5 | 187.8 | 191.4 | 194.4 | 197.2 | 199.5 | 200.8 | 200.0 |
| 1958 | 199.0 | 201.0 | 201.2 | 196.8 | 191.4 | 186.8 | 184.7 | 184.9 | 183.8 | 182.2 | 180.8 | 180.5 |
| 1959 | 178.6 | 176.8 | 173.5 | 168.4 | 164.4 | 161.4 | 155.8 | 151.2 | 146.2 | 141.0 | 137.2 | 132.6 |
| 1960 | 129.0 | 125.0 | 121.6 | 119.6 | 117.0 | 114.0 | 108.6 | 102.4 | 97.8 | 92.8 | 87.4 | 83.6 |
| 1961 | 80.2 | 74.8 | 68.8 | 64.3 | 60.0 | 55.8 | 53.1 | 52.4 | 52.3 | 51.8 | 50.9 | 48.7 |
| 1962 | 45.2 | 41.8 | 39.8 | 39.4 | 39.2 | 38.3 | 36.8 | 35.0 | 32.7 | 30.8 | 30.0 | 29.8 |
| 1963 | 29.4 | 29.8 | 29.8 | 29.0 | 28.8 | 28.2 | 27.7 | 27.2 | 26.9 | 26.0 | 25.8 | 21.3 |
| 1964 | 19.5 | 17.8 | 15.4 | 12.7 | 10.8 | 10.2 | 10.4 | 10.4 | 10.0 | 9.7 | 10.3 | 11.2 |
| 1965 | 12.0 | 12.3 | 12.7 | 13.8 | 14.7 | 15.2 | 15.4 | 16.5 | 17.2 | 19.4 | 21.9 | 23.9 |

COMPLETE SUMMARY OF MONTHLY MEAN VALUES OF SUNSPOT NUMBERS AT ZURICH

| Year | Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sep. | Oct. | Nov. | Dec. |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1954 | 0.2 | 0.5 | 10.9 | 1.8 | 0.8 | 0.2 | 4.8 | 8.4 | 1.5 | 7.0 | 9.2 | 7.6 |
| 1955 | 23.1 | 20.8 | 4.9 | 11.3 | 28.9 | 31.7 | 26.7 | 40.7 | 42.7 | 58.5 | 89.2 | 76.9 |
| 1956 | 73.6 | 124.0 | 118.4 | 110.7 | 136.6 | 116.6 | 129.1 | 169.6 | 173.2 | 155.3 | 201.3 | 192.1 |
| 1957 | 165.3 | 130.2 | 157.4 | 175.2 | 164.6 | 200.7 | 187.2 | 158.0 | 235.8 | 253.8 | 210.9 | 239.4 |
| 1958 | 202.5 | 164.9 | 190.7 | 186.0 | 175.3 | 171.5 | 191.4 | 200.2 | 201.2 | 181.5 | 152.3 | 187.6 |
| 1959 | 217.4 | 143.1 | 185.7 | 163.3 | 172.0 | 168.7 | 149.6 | 199.6 | 145.2 | 111.4 | 124.0 | 125.0 |
| 1960 | 146.3 | 106.0 | 102.2 | 122.0 | 119.6 | 110.2 | 121.7 | 134.1 | 127.2 | 82.8 | 89.6 | 85.6 |
| 1961 | 57.9 | 46.1 | 53.0 | 51.4 | 61.0 | 77.4 | 70.2 | 55.8 | 63.6 | 37.7 | 32.6 | 39.9 |
| 1962 | 38.7 | 50.3 | 45.6 | 46.4 | 43.7 | 42.0 | 21.8 | 21.8 | 51.3 | 39.5 | 26.9 | 23.2 |
| 1963 | 19.8 | 24.4 | 17.1 | 29.3 | 43.0 | 35.9 | 19.6 | 33.2 | 38.8 | 35.3 | 23.4 | 14.9 |
| 1964 | 15.3 | 17.7 | 16.5 | 8.6 | 9.5 | 9.1 | 3.1 | 9.3 | 4.7 | 6.1 | 7.4 | 15.1 |
| 1965 | 18.5 | 14.3 | 11.3 | 6.8 | 26.4 | 15.5 | 11.9 | 8.6 | 16.3 | 21.2 | 15.5 | 17.0 |
| 1966 | 26.7 | 23.5 | 24.5 | 47.5 | 43.7 | 46.4 | | | | | | |

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Book Review

MULLARD VOLTAGE REGULATOR (ZENER) DIODES

This book should quickly become a standard reference for everybody interested in electronics. Although voltage regulator diodes are mainly of use in transistorised equipment, they are also very useful in valve circuits.

Most of us have encountered the problems associated with the lower limit of 70v. for gaseous regulator tubes—voltage regulator diodes completely fill the gap from 0 to 70v.

This book completely covers the subject including characteristics of voltage regulator diodes in general and the Mullard range in particular; voltage reference circuits ranging from a simple stabiliser to a complete bench power supply for transistor circuits; voltage shifting circuits; voltage clipping circuits; and miscellaneous applications such as bias circuits, video amplifier, instrument protection, and non-linear function generator.

The book is available from all Mullard offices throughout the Commonwealth, retail price being 85 cents, postage 7 cents.

NEW CALL SIGNS

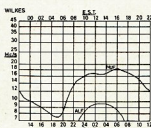
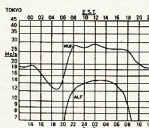
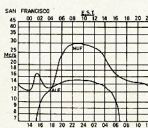
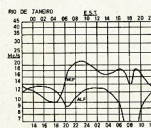
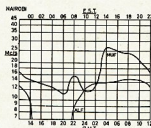
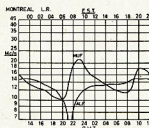
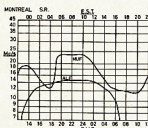
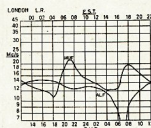
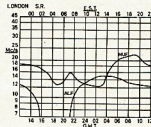
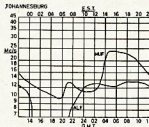
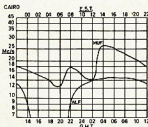
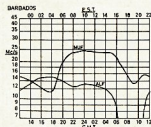
MAY 1966

- VK2BAI—C. L. Matthews, 4 Potts St., Kingsgrove.
 VK2BGK—G. S. Kiernan, C/o. O.T.C. Receiving Station, Bringley.
 VK2BHX—W. R. Boydew, 108 Bayview St., Warners Bay Heights.
 VK2ZEC—E. A. Chalker, Telopea Rd., Hill Top.
 VK2ZFK—P. A. Kerr, 32 Russell St., East Gosford.
 VK2ZRV—F. R. Forrester, 175 Margret St., Orange.
 VK3BET—M. L. Bartlett, 11 Ranelagh Dr., Mt. Eliza.
 VK3KJ—J. R. Adamson, 76 Shafer Rd., Blackburn North.
 VK3ZND—J. D. Vivian, 19 Thurliegh Ave., Croydon.
 VK3ZRC—P. D. Robertson, 10 Bath Rd., Burwood.
 VK3ZS—G. F. Coward, 333 Buckley St., Essendon.
 VK3ZSR—A. C. Greening, 3 Ferguson St., Ascot Vale.
 VK3ZST—W. D. Brain, 179 Gladstone Rd., Dandenong.
 VK3ZTU—A. L. Tuckerman, P.O. Box 43, Kangaroo Flat.
 VK3ZVV—R. J. Halligan, 41 Windsor Ave., Mt. Waverley.
 VK3ZXO—T. P. J. Cosway, 102 Christmas St., Northcote.
 VK3ZYD—L. De Stefano, 13 Sheales St., Dandenong.
 VK3ZZG—I. R. Gillard, 25 Elliott Ave., Balwyn.
 VK3ZZO—D. S. Thomas, 24 Albert St., Mt. Waverley.
 VK4EP—P. Ellis (Rev. Bro.), St. Patrick's College, Shorncliffe.

- VK4LH—L. Grimshaw, 36 Leigh St., West End, Townsville.
 VK4ZGP—C. R. Phillips, 8 Chatham's Post St., Enoggera.
 VK4ZLB—B. J. Byrne, 17 Boyd St., Wilsonton, Toowoomba.
 VK4ZMW—M. J. Whittle, 18 Chisholm St., Sinfarod, Brisbane.
 VK4ZRL—R. D. Ross, C/o. Commonwealth Bank, Rockhampton.
 VK4ZTP—T. F. Armstrong, 2a Phillip St., Toowoomba.
 VK5CU—D. Clift, Flat 1, 25 Fitzroy Tce., Fitzroy.
 VK5PX—D. A. Millar, 90 Portrush Rd., Payneham South.
 VK5ZAU—B. J. Bryant, 1 Kilner Rd., Greenacres.
 VK5ZFW—A. S. White, 70 Devereux Rd., Beaumont.
 VK5ZHP—M. G. F. Huizinga, 14 Birch Gr., Derranacourt.
 VK5ZNN—T. G. Norris, Port Clinton.
 VK5ZTC—Adelaide Teachers' College Electronics Club, Kintore Ave., Adelaide.
 VK6GW—W. B. Nielsen, C/o. W. H. Pinniger, Ocean Beach Rd., Denmark.
 VK6VH—L. W. Hoobin, 9 Lillian Ave., Applecross.
 VK7ZPS—H. P. Schulz, 14 Liverpool Cres., West Hobart.
 VK8JD—J. F. Dalstead, 5 Ninth St., Lae, N.G.
 VK9ZCL—C. Lee (Rev. Bro.), Catholic Mission, Mt. Hagen, N.G.



PREDICTION CHARTS FOR SEPTEMBER 1966



(Prediction Charts by courtesy of Ionospheric Prediction Service)

SIDEBAND TOPICS

When you decide to spend a lot of money on a modern s.s.b. transceiver, you are actually buying two things, an s.s.b. transmitter and an s.s.b. receiver, combined in one package. Most transceivers now available can transmit potent good quality signals, there are no bad ones as their manufacturers would soon be out of business. Sometimes the outer appearance or finish of a set will influence a choice, but what is frequently neglected and taken for granted is the receiver performance. All transceivers are used much more for reception than transmission and it is the receiver in a Galaxy V. that makes this set so attractive.

The GALAXY V. RECEIVER is:—

- (a) The most sensitive one of the lot.
- (b) The one with the lowest background noise.
- (c) The only one with a near perfect a.v.c. action.

One can copy stations on the Galaxy V. that simply are not audible above the receiver noise in other sets. Except in very noisy locations there is absolutely no need to "fiddle" with its r.f. gain control, it can always be left at maximum receiver sensitivity. The receiver just cannot be overloaded, its a.v.c. system is better than any other s.s.b. receiver of my knowledge, none excepted. Why? Because of its product detector circuit, first developed by Galaxy, using a "frame grid" pentode, now copied and used in the Drake transceivers. This detector can handle a larger range of signals than any other detector.

Furthermore, the Galaxy V. has selectable sideband switching without shift in operating frequency, a system found only on much more expensive sets. Also, the accessories like VOX, crystal calibrator and external v.f.o. are cheaper than for other makes. The external v.f.o. does not need an extra adaptor, doubles the usefulness of the transceiver in separating the transmit and receive channels at will. In some mobile applications the smaller size of the Galaxy V. can also be a distinct advantage.

The best advice is: Ask the man who owns one!

GALAXY V. all-band S.s.b. Transceiver, with heavy-duty matching power supply/speaker unit \$600
HY-GAIN Antennae:

14AVQ, 10-15-20-40 mx Vertical Antenna, 18 ft. tall, self-supporting, 4-band groundplane \$44

18AVQ, as the 14AVQ, but also for 80 mx, 32 ft. tall, requires 2-3 sets of guys (supplied) \$70

TH3JR 3-element 10-15-20 mx Junior Tri-band Yagi Beam \$96

TH6DX 6-element 10-15-20 mx Senior Beam, 4 el. on 10 mx, 3 el. on 15-20 mx, 24 ft. boom \$200

ALLIANCE & C.D.R. Antenna Rotators, control-indicator units for 230v. included \$55 to \$180

AUTRONIC Transistorised Automatic Keyers \$70

MOBILE 12v. d.c.-d.c. Power Supplies, 300 and 500w. \$100/\$120

WEBSTER Bandspanner All-Band Mobile Whip, continually adjustable to frequency, complete with mounting assembly \$48

★ Expected next month: 572B Triodes! All hard-to-get types of transceiver tubes in stock.

★ For the home builder: Crystal Filters, Air Trimmers, Jackson Reduction Drives, 8.0 and 9.0 Mc. Crystals, etc.

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Telephone: Springwood 51-1394

Diodes in Power Supplies

Editor "A.R.," Dear Sir,

In the July issue of "A.R.," Phil Williams has written a very interesting article on power supplies for Sideband. I desire, however, like to say that I do not agree with all of his design considerations concerning the use of silicon diodes.

The R.C.A. Transistor Manual (p. 52) states that if no transient suppression is used, it is desirable to use a diode p.i.v. safety factor of three or four times the expected peak working voltage, because of switching transient overvoltages generated in the power transformer. Even when transient suppression is used, a safety factor of at least 1.5 is required, because "suppression" is not the same as "elimination". Transient suppression can be obtained simply by putting about a 0.01 μ F. condenser across the primary of the power transformer. When the primary is run from the 240v. mains, that condenser ought to be rated for at least 600v., since the condenser must withstand the transients it is trying to suppress.

In addition to the R.C.A. Transistor Manual, this subject has been discussed in the Selected Semiconductor Circuits Handbook, G.E. SCR Manual, and in numerous periodicals, eg. "Equipment Exchange Bulletin". And yet one frequently sees published designs which lack that all-important condenser. Why? Possibly because one can indeed ignore the existence of transients for a long time, until that one time when you turn the supply on (or off) at the wrong time in the cycle—then poof! This is taken stoically with the same attitude that one replaces valves. But a properly rated diode should never need replacement. And you can be reasonably sure that the one time it blows will be when you turn on the rig just after hearing a W1 call CQ on 2 metres.

Phil Williams suggests that a 400v. diode be used for each "130v. of transformer output," presumably meaning 130v. r.m.s. coming from the transformer, but this means a peak of $130 \times 1.4 = 182v.$ 400v./182v. = 2.2 safety factor. This 2.2 is inadequate for power supplies not protected by the transient suppressing condenser, but excessive for ones that are protected. Excess safety factor means higher unnecessary cost when putting diodes in series for h.t.

But why put 400v. diodes in series for h.t.? Several of the advertisers in "Amateur Radio" sell diodes rated higher than that, and two of them sell 2,000 p.i.v. diodes at a comparatively reasonable price; this even makes it practical to replace 866s with diodes, for obvious reasons. The only justification for putting a lot of diodes in series, is to save money. Sometimes this is better done with a string of diodes, or a few; before deciding on a design, it would be wise to see whether requirements are better filled by a few h.t. diodes rather than many m.t. ones.

The p.i.v. applied to a half wave diode feeding a condenser input filter is twice the peak voltage coming from

the transformer, because the condenser adds to it on the off cycles, not to mention the fact that a half wave circuit suffers far more from transient overvoltages than a full wave design; in the latter case the transformer is loaded on the off-cycle, but for the half wave it isn't. Well, if VK5NN's Fig. 2 actually feeds 240v. r.m.s. to his half wave 400v. diode, he is in trouble: 240v. r.m.s. = 340v. peak. $2 \times 340v. = 680v.$ That is rather a lot to ask from a 400v. diode, not to mention safety factors.

Choke input filters can be responsible for horrid transient voltages too. With valves this was no great problem (unless running a mercury vapour one near its limits!), but with silicon diodes it can be critical. Again, the cure is simple: a 0.1 μ F. condenser in series with a 1K resistor, shunted across the choke. If I were you, I'd draw in that R-C across all diagrams of chokes following silicon diode rectifiers. The 0.1 μ F./1K should work in most cases. More detailed considerations can be found in the silicon diode article in the January 1965 issue of "QST" or reprinted in "Amateur Radio" several months later. [August 1965.]

Part of the confusion with respect to safety factors comes from the ambiguous or conflicting ratings of diodes. Australian and British commercial firms tend to give their diodes a working rating which includes a 1.5-fold safety factor in it already; American or surplus merchandise tends to be rated closer to "absolute maximum". Thus, an OA210 is nominally 400v., but its absolute rating is about 600v., which explains why it can be used with success on 240v. mains. Similarly the BY100 is nominally 800v., but its maximum voltage is given as 1,200, and is probably even better.

I do not think that it is desirable to include the p.i.v. safety factor in the nominal voltage rating of a diode because, as I discussed above, the actual safety factor needed depends on the circuit used. I think that it is more sensible to rate diodes explicitly at the "absolute maximum" value, making quite clear that this maximum is truly absolute and letting the experimenter exercise his own discretion in applying the devices. This discretion must include some knowledge of transient suppression, safety factors, and circuit behaviour; silicon diodes are neat and cheap, but they are not nearly as simple and uncritical as selenium metal rectifiers or valves. See "Silicon Diodes and Common Sense," in the September 1965 issue of "CQ".

While I am about it, I might mention that because of the violence of the switching action, silicon controlled rectifiers operating from a transformer can require a p.i.v. safety factor of 2 or more, even when the a.c. input is transient suppressed. Design for suitable R-C suppressors as discussed in the "Mini-watt Digest" for January 1965. SCR's working directly from the mains are somewhat less critical, but it is still hazardous to use an SCR directly on the 240v. (r.m.s.) mains unless it has a p.i.v. rating of at least 500v., preferably 600v.

To a certain extent, the application of a diode p.i.v. safety factor will de-

pend on the reliability one needs. I have run diodes with a 1.1 safety factor when powered directly from the mains, with no sources of inductive disturbance nearby. But I also cooked a bunch of diodes in a rather h.t. circuit using a safety factor of 1.7, because the transformer was unusually inductive, or something. In this case I solved the problem by applying the formula used when putting a resistor in series with the transient suppressing condenser. R-C combination is more effective than C alone, because the capacity used is appreciably larger. But it can come to grief unless the formula is used, because of the danger of shock-excited resonance of the transformer with the condenser, if the latter is too large. The formula can be found in the "Mini-watt Digest" for July 1962, or in several of the data sheets in the Mullard "Technical Manual" Vol. 4 for diodes. Approximate values are given in the February 1965 issue of the "Equipment Exchange Bulletin," and the principles involved are discussed in the May 1965 "E.E.B."

—R. L. Gunther, VK7RG.

[The above letter was referred to VK5NN, whose reply follows.—Editor.]

Editor "A.R.," Dear Sir,

On first reading VK7RG's letter I had thought of having done something dreadful in the S.B. Notes for July, but on consulting Fig. 2 I was relieved to see that I had not done the dirty deed of which I was accused. If Lee sticks his chin out he will then see through the lower portion of his bifocals, that there is only 120v. applied to the rectifier in the bias circuit, and not 240v.

Following a loud "Touche!" I will now proceed to agree with him, and ask his forgiveness for omitting all the fuses, filters (r.f.), bleeders, milliammeters, and the 1,000 pF. capacitors across the diodes, all of which I have used in my own equipment (see "The Tetra-Linear," May 1964 "A.R.").

My own station uses a total of 82 silicon diodes in various configurations and I have only ever damaged one on a choke input circuit. This was replaced and an R-C circuit connected from choke input terminal to ground or as he suggests, across the choke—but I prefer to ground them. An 0.05 μ F. 1,000v. paper condenser and 1.2K resistor were installed.

The figure of 130 volts a.c. per 400v. p.i.v. diode was published by Mullard and Philips in the data sheets for the OA210 rectifier, and I have used these, 1N1763s, HR255s, RS25AFs and possibly others in series, always with 330K and 1,000 pF. across each to equalise surges and back voltages.

We are fortunate that higher voltage rectifiers are available now for less than I paid for my original OA210s. By all means use them with as much safety factor as you feel you can afford. Manufacturers always tend towards the use of I.C.A.S. ratings, don't we.

The Sideband Notes for July were intended to be a source of a few ideas which might prove useful for giving the voltages for s.s.b. equipment. The tips in Lee's letter are worthy of consideration, too.

—Phil Williams, VK5NN.

Amateur Radio, September, 1966



Sub-Editor: ALAN SHAWSMITH, VK4SS
35 Wynnot St., West End, Brisbane, Qld.

It would seem that the Don Miller stint from Heard, I. was not a success in the first place. Two thousand QSOs were made, mostly with W's. Only 30 Europeans were worked and very little else. The question that comes to mind is, was it all worth it? It's only a guess but it appears the venture cost more than a dollar per QSO.

NOTES AND NEWS

Easter Is: Jose C20AC is about to be on at irregular times on 7001. Try listening 0500Z.

Nepal: Terry 2V1BG reported on 14100 s.b. Worked here 1800Z. QSL to H.Q., British Gurkha, L. of C. Dharan.

Oland Is: SM8ENU/7 on now 14135. Try the SR for this one, however, he may be QRT by the time this reaches you.

Heng Kong: Luke VS8AZ. On fairly regularly. Listen around 1400Z on 14195.

Marens Is: Now reported QRV again. Try 14200 from 1800Z.

Andaman Is: Hedge VUDDIA still working them daily on 14015 around 0130Z.

Glorieuses: Jose CR1GF ran into generator trouble on the first leg of proposed Xpedition, consequently he doesn't expect to get on from Aldabra and Tromelin until late August at the earliest. Will then go to Farquhar, where he already has a base.

Pantelleria: IPIAA and IPIJT expected to show soon from Khamma. If you do manage to QSO these stations, QSL to Dave Nono, 1434 Bridges St., London, Ontario, Canada.

Pitcairn Is: Tom is now to be found more often on 14175, 0600Z. He still keeps to his other schedules, however, i.e. 21069, 2200Z. Sometimes 21 c.w. later.

Prince Edward Is: VE1AKZ is said to be on from this spot very soon for period approx. 5 weeks. No times or frequencies available.

(Much of the above by courtesy of Geoff Watts.)

Gurin—N. Coast Territory: 10RB on 14250 minus count for D.X.C.C. Try around 0600 or 1300Z.

International Ken-Tiki: Report to hand says that five men are setting out on a raft to travel from Peru to Australia. In the wake of the Norwegians and William Willis's "Age Unlimited." A Ham rig is supposed to be aboard. Date of departure is at present fixed for end of August. Any more information on this adventure would be greatly appreciated (so please chaps keep me posted).

Desroches: Plans for this spot also went astray. Transport difficulties. They may try it again in a couple of months.

Stockholm: Originally prefix SM3 but now SM8. Several are QRV. Just in case you didn't know.

Ceylon: 457PB on 14110, 1800Z. QSL K2MGE/. Also very active is 457DA on 7/14 c.w. Best time for the former is 1400Z or 1800Z.

American Samoa: Active as now W5WU/KS6, 1400Z. Duration of operation not known.

Bonin Is: This spot now has two ops. and their joint QSL manager is K6ZDL. Modes are 1 and 14 c.w./s.b.

Kerguelen: FB8XX active daily 14140, 0400Z.

Bahrain: Roger MP4TBO should show up any time now. 14 c.w./s.b. Duration of operation not known. QSL VE1AKZ.

Rare Ones Coming Up: Information to hand says that Ack and Don are planning operation from KC4, P08 Clipperton, ZA, YI, PY0 and more in the not too distant future. Keep an ear out for these frequencies.

(Much of the above by courtesy of Bill WAZEPF, Ed. LIDXA.)

Turkey: As reported previously TAEKX is active 14 c.w. and been worked here. TAAZA has shown up on 14 s.b., and said to be audible on LP from 1400Z.

India: Previous notice on this place was that 3V8EU would commence operation. Now it seems it was all a foney. Another report to hand, however, says that W5WU is about to cause a stir. No further information.

Juan de Neva: Further information from CR1GF says that he will endeavour to include this rare one in his itinerary probably

about next October or earlier if possible. Call will be FR7Z.

Haiti: HH0DL is QRV 14190 and listening on 14210.

U.S.S.R.: If the call USARTEK raises your blood pressure, forget it. QTH is Crimea. Box 98, Moscow, for a QSL. QRG is 14240 s.b. also 14 c.w. after 0400Z.

Portuguese Guinea: CRKDK worked 2100Z. (Right alongside frequency of Tom VRETO and about the same time, 2200Z.)

(The bulk of the above by goodwill of Joe W4MVB, Ed. Fla DX'er.)

Jan Mayen Is: Latest from here says that some four or more QSLs are busy on the air. LA2IK, LA2AK, LA2KI, LA2CI, all on 14 c.w. The latter also has s.b. all bands.

Spitzbergen: LA4FG/P is a loner from this spot at present.

British Gulana: 4U2BZ said to be operating 14 c.w. Try 14075, 0500Z.

Wallis Is: Robert FWSRC as reported before mostly at week-ends. 6700Z around 14340 Kcs. QSL P. T., Mata-Uia, Wallis, New Caledonia.

Branel: Another one from here is VSJJC, 14 c.w., low end of band around 1300 ZQST. Sgt. Cooper, Gurkha Sig. Sqdn., c/o P.O. Box 777, Singapore.

South Orkneys: LU1GZ is active on 21251 c.w. (yes, c.w.). I think he will also work s.b. stations on this frequency.

(From Jim G3UGT, Ed. Airwaves.)

Uruguay: Remember Enzo CX2EJ. Sadly the sun has set on him for his last of this "old-timer" has just passed away at the age of 72 years without receiving a single VK QSL. A letter from his son to Chas. VK4UC tells of this. Enzo in his time worked quite a few VKs.

Boettlegers: If recently you worked F1BCC or K54AC, they are probably phonies. (VK4UC.)

ACTIVITIES

Ken VK3TL reports working these juicy ones over the past week or two. All 14 Mc.: EA8EZ (Canary Is.), F1PIL, G3ACH, H1RCP, LX21W, ON4NM/LN, ON1XA, PY1YR, VO1IB, VO1BG, VPIHR, VP2AA (Antigua), VP2AK, HAFPC, VUDDIA (Andaman), JADKX, NZ2AAE, Q9SGR, plus others. Best QSL received were: HK0KL, SL7CA, 9V1MT, V6MYI, COBMN, HRIJAP, ZP5LS, GJENEX, XV5AA, OH0VY, EY1USG, 6Z4FB, FWSGZ, LA1KED (I.P.L.), GWNZ, HCRJG, FPGCV, GCRHT (Guernsey), KS4CA (Swan Is.).

Dud VK4MY reports contacts on the Gold Coast only fair and been QRL working on Tx and aerial. He logged 14 c.w.: UA4HW 0400Z, UREBX 0330Z, 95VSWU/K3C 0150, Z56RM 0700Z, KR6WT 0545, UR2DE 0130, 6Y5BB 0645, and more.

Peter VK4PJ buys with things other than A.R. but manages these choice ones around 14125. s.b.: HBXAL, YV5CMQ, FBZA, HK4PFZ, VE2PA, SV1BH, HB9QO, HRIKS. Mostly around 2100Z.

QTHs

VP2AA via VE3ACD; F8CVC, W2GKZ; PY1YR, W2GHI, K2XV, W2GHIK; 3ADKX, K6CYG; VPIHR, Stann Creek Valley, British Honduras; ON4WM/LX, K2MYR; VPFP6; LA2VIL, 904QR, Box 10,961, Kinshasa, Republic of Congo.

(My thanks to Ken VK3TL for these—A.L.)

SUMMARY

Recently "CQ" magazine held what might be termed a miniature Gallup Poll on the question of the Ham and his equipment. While, for obvious reasons, the latest transceiver type unit was immensely popular, it was surprisingly found that quite a number still pre-

ferred to build their own equipment. In fact, on a population increasing basis, the home-brewer was more than holding his own.

While there is something to create, and a challenge to go with it, there will always be triers. The end-product, most certainly will not look as well, and probably will not function as efficiently as the factory job, but it will provide double satisfaction. The making and the using.

Henry Ford, one cold and frosty morning, was found yapping about bread-crumbs. When reminded he did not have to do it, his reply was, "Yes, but this way, it warms me twice."

My thanks this month to Editors Jeff Watts, Bill WAZEPF, LIDXA, Joe W4MVB, Fla. DX'er, Jim G3UGT, Airwaves, and from Chas. VK4UC and S.W.I. C. Thorpe, 73, Al VK4SS.

W.I.A. V.H.F.C.C.

| Con- fir- ma- tions | 144 Mc. 50 Mc. | |
|------------------------------|----------------|-----|
| 1 | VK3GQ | 114 |
| 2 | VK3QV | 215 |
| 3 | VK3HE | 102 |
| 4 | VK3HE | 118 |
| 5 | VK3TLZ | 112 |
| 6 | VK3EB | 300 |
| 7 | VK3EB | 132 |
| 8 | VK2ABR | 177 |
| 9 | VK3ZAX | 100 |
| 10 | VK3ZAX | 100 |
| 11 | VK3ZAX | 157 |
| 12 | VK4ZAZ | 847 |
| 13 | VK3BQ | 185 |
| 14 | VK3BQ | 204 |
| 15 | VK4HD | 114 |
| 16 | VK4ADT | 219 |
| 17 | VK4ADT | 163 |
| 18 | VK3BN | 110 |
| 19 | VK2ASZ | 100 |
| 20 | VK3KX | 100 |
| 21 | VK3TLZ | 104 |
| 22 | VK3ZHF | 402 |
| 23 | VK3GQ | 118 |
| 24 | VK3ZU | 103 |
| 25 | VK4ZCH | 101 |
| 26 | VK3AU | 107 |
| 27 | VK3KX | 100 |
| 28 | VK1VP | 100 |
| 29 | VK4ZAL | 100 |
| 30 | VK4ZAL | 100 |
| 31 | VK4ZLG | 100 |
| 32 | VK6ZDS | 108 |
| 33 | VK3ZCR | 107 |
| 34 | VK3ZG | 104 |
| 35 | VK4ZK | 103 |
| 36 | VK3WV | 103 |
| 37 | VK3WV | 214 |
| 38 | VK6VY | 102 |

Correspondence

Any opinion expressed under this heading is the individual opinion of the writer and does not necessarily coincide with that of the publishers.

C.W. PRACTICE
Editor "A.R." Dear Sir,

For the benefit of those who really do wish to pass the Morse Exam., the following information may prove of interest.

Sydney radio VHP/VIX broadcasts 24 hours a day for ships. Traffic lists consisting of ships' call signs in alphabetical order, followed by traffic, are broadcast at 0001, 0401, 0801, 1201, 1601 and 2001 G.M.T. on these frequencies: 4296 Kc, 6428.5 Kc, and 6478 Kc. Weather messages in plain language and code groups of five figures are broadcast on the same frequencies at 0130, 0330, 0630, 1030, 1730 and 2130 G.M.T. Speeds range from 16 to 20 w.p.m. The ship/shore frequencies in the region of 5390 and 8400 Kc. provide useful practice.

San Francisco Radio stations KPH and KFS both give daily press releases at 1620 G.M.T. on 6265 Kc, and KPH at 1900 G.M.T. on 6488 Kc. KFS is 25 w.p.m. and KPH is 28 w.p.m.; those with tape recorder facilities can record these and play them at half speed.

You may care to publish this information for the benefit of those who really do wish to pass and do not wish to attend a class. For those who want extra last minute practice, VHP 4425.5 often runs coded message tests to ships at 18 w.p.m. at 8.30 a.m. most mornings.

—John H. Smith, VK3JQ.

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His thoughts are always far away, With dots and dashes and 3GK, His family knows that first of all He must answer at once the "CQ" call. Crackles and voices from near and far,

Echo whenever his door's ajar.

At meals he's only half-way here, His mind's on the voice only he can hear.

Sunday morning's the sacred time, To call him then would be a crime. I sometimes long for the good old days Before Marconi and radio waves, —Mrs. S. M. Gillespie.

CONTEST CALENDAR

10th/11th Sept. — W.A.E. Contest (Phone).

1st/2nd Oct. — VK/ZL/Oceania DX Contest (Phone).

8th/9th Oct. — VK/ZL/Oceania DX Contest (c.w.).

15th/16th Oct.—R.S.G.B. 21/28 Mc. Telephony Contest.

29th/30th Oct.—R.S.G.B. 7 Mc. DX Contest (Phone).

12th/13th Nov.—R.S.G.B. 7 Mc. DX Contest (c.w.).

19th/20th Nov.—R.S.G.B. 2nd Top Band (1.8 Mc.) Contest.

10th Dec./15th Jan.—Ross Hull Memorial V.H.F. Contest.

11th/12th Feb.—John Moyle Memorial N.F.D. Contest.

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FEDERAL AND DIVISIONAL MONTHLY NEWS REPORTS

(SEND CORRESPONDENCE DIRECT TO DIVISIONAL REPORTER NAMED AT PARA. END)

FEDERAL QSL BUREAU

WPFIO, Will Grob, is looking for an Australian to pay pal for his daughter Diana, who is 16 years of age, and doing her last year at high school, may be reached at 115 East Liberty St., Columbia, Illinois, U.S.A. RAG, RASHBY, who was a regular visitor to Australia when radio officer on the M.V. Besumont a few years back, was a delegate to the I.A.R.U. Region 1 conference in Yugoslavia during May. Rag sends his best wishes to his many VK friends.

QSLs for the final stages of Gus Brown's last DX-pedition and mainly for West African areas, were recently received from WZOHK.

Further to paragraph these notes in "A.R." regarding CXZAJ, advice has now been received from his son that this fox was based away suddenly on 20th June. CXZAJ made 72 years and death was due to heart trouble. His son is finalising all QSL obligations.

All QSLs for YOF Hans may be sent via: YOF QSL Bureau, P.O. Box 100, Timisoara, Romania.

Ray Jones, VK3RJ, Federal QSL Manager.

FEDERAL AWARDS

AUSTRALIAN DX CENTURY CLUB AWARD

At the recent Federal Convention it was decided when determining the highest twelve in each section of the D.X.C.C. in future, allowance is to be made for "deleted" countries, of which 24 are currently involved. Clauses 2.2 of the Rules provide "Deleted" a country be deleted from the Countries List at any time, members and intending members will be credited with stations until the date of contact was before such deletion." This practice will continue.

Two tables will accompany the listing of the top twelve in each section in future. Position in the list will be determined by the first number shown which will represent the participants in the section. Any credit given for deleted countries. The second number shown will represent the total D.X.C.C. credits including deleted countries, in accordance with the Rules.

The first such list will appear in "Amateur Radio" next month.

A. Klassick, VK3BK, Federal Awards Manager.

NEW SOUTH WALES

The July monthly meeting of the N.S.W. Division, held at Wireless Institute Centre on Friday evening, July 22, took the form of an Auction Night.

Such events have always been popular, never failing to draw good attendances, and about 150 members and visitors were present on this occasion.

Chairman Tom O'Donnell, VK3OD, dispensed with the usual preliminaries in about 10 minutes. The first business before the meeting was a motion by the Federal Councillor, Pierce Healy, VK3AFQ, that the minutes of the recent Federal Convention be ratified, with the exception of an action dealing with the proposed constitution. This was seconded by Bill Lewis, VK3B, and carried without discussion.

The following applicants were admitted to membership of the Institute: M. O'Grady, P. Payne, C. Campbell (VK3BLC), P. C. Nieuwendyk, N. Spratt, G. T. Pike (VK3ZPG), R. G. Turner (VK3ZTR), T. S. Mayne (VK3ZM), the Nepean District, A.R. Club, A. E. Prentice, Leonard Deitch, R. C. Milton (VK3ZMM), Dick Treacy (VK3BAJ).

Proceedings were then handed over to Noel Miller, VK3AQH, who, as on past occasions, carried out the duties of auctioneer both efficiently and with a minimum of fuss. He attempted to extract the D.B.'s from the audience. This proved a rather difficult task, for the spite of the fact that there was a considerable buyer resistance. High reserve prices on some equipment was one deterrent to brisk bidding, but even so, it would appear that many of those present came along merely out of curiosity, or perhaps in an effort to

clear their own shackles of all manner of junk, at the same time resisting the usual Amateur impulse to find the shack again with someone else's doorsteps.

This attitude is in direct contrast to the auctions held immediately after World War II, when Disposal equipment was first making its appearance. How well we remember an auctioneer of those days being almost knocked off his perch by the rush of bids, and the bidding was usually closed when he considered a sensible amount had been received. It seems those days are gone for ever.

About 11 p.m. the auctioneer called it a night. He had been assisted by Warwick Johnston as recording clerk, Bill Shakespeare, VK2AGF, as official extractor of dollars from purchasers, while equipment handlers were Norm Cameron, VK3ZM, Kevin Trevitt, VK3BZU, and Ivan Agar, VK2AIM. A vote of thanks to Noel and his band of helpers, moved by Bill Lewis, VK3BY, was carried by acclamation.

Before we get too far from the subject of auctions, we are seeking the purchasers of a receiver and a wave-meter offered for sale on behalf of the late John Peehi, VK2WJ, at the June, 1965, auction. We are holding a handbook for the former and cash for the latter, and these may be had from Ivan Agar, VK2AIM, telephone Sydney 88-5179, or address as in the callbook. Alternatively, if any reader can advise the identity of these purchasers it would be appreciated.

We are sorry to report that the Divisional President, Tom Dorrance, VK3O, died during the month while on Institute business, when he stepped into a hole on a badly weighted chair. He had been suffering from various aches and pains, he was confined to the cot for a day or so, and left the July monthly meeting in a very weak condition. Incidentally, Tom assured us that he was quite sober at the time, and he also assures us that the Shire Council which controls the offending footpath has received a few caustic comments.

Divisional Council has received a very good suggestion from Mona Swinton, VK3AXS, that a display of the members' hobbles (other than radio). The idea has been well received and the Education Officer, Harold Burdett, VK3BAJ, is planning to organise the display, which it is hoped will be held early next year.

The W.I.C.E.N. group held an exercise on Sunday, July 24, in the Berrima district, when there were 12 mobiles among the 17 call-signs in attendance. Much useful experience was gained by the operators as a result of this day out, one feature being the excellent coverage from VK4WJ on 146 Mc. fm. Using 50 watts to a ground plane antenna, the station was received at 5.8 south of Berrima and two-way communication was maintained between Dural and Mittagong. The W.I.C.E.N. Committee had a meeting during the month with the N.S.W. Civil Defence Director, and the results of this visit to have been submitted to the August meeting.

The Far Northern Radio Club members and their families assembled at Lennox Head on 24th July for a group picnic and hamfest. After a picnic lunch, the members got their heads together and held this meeting, and we would like to commend this idea to other county clubs and city clubs, for that matter—for it is an excellent way to have a family get-together and a meeting at the same time.

The VK2 Divisional Morse practice is thriving. Ern Hodgkins, VK2EH, who now conducts the service, reports increasing appreciation for the service. W.I.C.E.N. nightly Morse practice on approximately 3550 KC, carried out by Doug, Courtney, VK2AUC, and his hand and foot operators, is also received with much appreciation in several States.

SILENT KEY

It is with deep regret that we record the passing of:

VK2PD—Jack D. Sibbald.

VK3UX—Gordon Weynton.

VK3UX—Leslie Wallbridge.

Many Amateurs on the air today owe their success in the A.O.C.F. to the dedicated work of these volunteers and the services they maintain.

Howard Lilley, VK2AYT, was the envy of his mates when he took off late in July for the U.S.A. about two weeks. Howard is on the staff of ABC-TV Channel 2 and while in the States will undertake a course of study in connection with his work.

Our Zone 2 Officer, Max Francis, VK2BKM, has changed his QTH, and for the information of all concerned he is now to be found at 83 Kingston Street, Scone.

Members of the N.S.W. Divisional Council, and indeed all thinking Amateurs, are most concerned at the lack of response in this State to appeals for I.T.U. Fund donations. It is very difficult to understand the mentality of those individuals who apparently think so little of their hobby that they would literally throw it to the wolves. It is known that while this Division is scratching along with little more than 25 per cent. of its quota, after three years of effort and appeals, the opposing forces are leaving no stone unturned in their efforts to prove that bands are not being used efficiently and warrant their retention by the Amateur service. And this is not confined by any means to the I.U. band plan, but extends to the use made of them, are being scrutinised very closely by those who covet them. If we are to compete with the I.T.U. interference with any frequencies worth having, there are two things we must do—and do quickly. First, we must improve our bands every opportunity, and rally to the call for donations so that we will have a representative at Geneva for the next year in jeopardy as it is, but with no one else to spare for it would be hopeless. T3, Ivan, VK2AIM.

HUNTER BRANCH

Although many dislike the winter for its short days and cold mornings, it goes almost without question that this season is the ideal time for the Hunter Branch to progress. It seems so in the Branch area anyway and many are the reports of newly-kindled activities. The branch programme for 1965 are now five stations in operation either fixed or mobile and one more at least, Henry Charles, VK3ZLH, has been given the go-ahead this. Charles ZLH also has been bitten by the desire to join the net operators and, having availed himself of a give-away priced unit is in the process of converting it to 146. Latest members to come up on the frequency are Des Z2DN and Jan Z2JO. Both have converted MR3 carphones to their use and Jan runs his mobile in the 6-volt horseless carriage known affectionately as the "Lurchmobile". It is a 1954 model and will connect the unit to the battery! In an attempt to trap more signals, Des has erected a 3-element beam antenna. When the recommendations and this has been copied by some others as well. It is possible now to hear 2W1 on 2 meg. line at good strength at my location. All this activity on the W.I.C.E.N. frequency will no doubt do a great deal of good and provide a core of skilled operators to help new entrants.

The presence of skilled operator-technicians is undoubtedly the reason for the success of the Cessnock Civil Defence radio network so many of our members are keen to know what is happening to the signal and how important a good aerial is then the case. It is a pity that many of our members are doing its job efficiently. This informed attitude is quite a long way removed from the amateur who merely "wonders" when a misguiding person who may be seen daily coveting to and fro in their high-powered auto and no-aving it at the rear. Or even those others who slide up and down the spectrum, Amateur bands included, with their war game chit-chat issuing from ill-adjusted 19 and 20 watt transmitters. The result is novelty will wear off and they'll give it away or else they'll become efficient and do some useful work. I am reminded while on the subject of a certain acting lanky-bank who after having been in the branch for but just a small amount of radio being severely reprimanded when seen using a resonant aerial on a vehicle seat. You'll see the foolish thing he did while in the bus of his official mind echoed the chorus, "The



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mittee on this score, after there had been another speaker with the same idea. Permission was granted, and possibly more will be heard later.

The technical side of the meeting was then commenced, and the subject for the night was "Transistors in communication receivers," the guest speaker being a tape recording by 2AB6, and a collection of slides displayed appropriate points to show just what could be done, and how. Ron 5K5, as programme organiser, manipulator of the slides and tape recorder, was suitably thanked for his efforts, and also asked to pass on the thanks of the meeting to the appropriate source, and one of the members asked if it would be possible to publish the circuits displayed in the Divisional Journal, and was assured that if at all possible efforts would be made to do so. Uncle Tom STL was one of the last to leave the meeting, and he arrived home at 10.15 p.m., so it seems that if the caretaker and his bound dogs are to continue to get their monthly frolic with the members, then I must start attending the meetings again, and if I might say so, reluctantly be forced to become controversial and difficult. 10.15 p.m.—I am ashamed and mortified! Come rain or shine, see 5GP always manages to attend meetings, and when you remember the distance he has to travel it speaks volumes. He seemed very interested in getting his quota of cards from the bundle Murray 5D3 brought in on behalf of George 5RX.

My special spy, who it will be remembered, is planted in Georgia Tech., Atlanta, Georgia, disguised as a statue in the garden, reports that I need not have any further worries that Bob (ex-SFU—now a WA) might be returning to VK and possibly going to VK3. He tells me that Bob is still coming home, but VK3 will come out on top after all, because the WRE is now prime favourite. Once again good has triumphed over evil—evil in this case being represented by VK3! Had quite a chat with "Sheep" 3DC at the last meeting and could not help but notice just how young and spry he looked. His appearance is very deceptive—he looks by far too young to be in the old-timer class, but it must be remembered that he cut his teeth in Amateur Radio back in the old 300 metre days, and there are not too many of those boys left now. He used to broadcast on Sundays, especially for the music lover, and his 20 or 30 part orchestra, out on the air court, will be remembered by many listeners of that era, the quality and general high standard when compared favourably with the commercial stations of that early time.

Talking of young old-timers, Arthur SHY was sitting next to "Sheep," and believe me, put these two in a bag and shake it up, and

you would never know which one fell out—honestly. Perpetual youth, I suppose!

Received a letter from an ex-VK5 who is at the moment residing in VK2, not licensed these days, who said, among other things, that he had only just found out that I was the perpetrator of the VK5 notes, and was amazed somewhat because he did not remember me as much of a chameleon school. I was cut to the quick, this flattery, because if my correspondent had only stopped to think he would remember me as always getting high marks on spelling, arithmetic and grammar, and nothing of geography and mathematics. Surely he must remember the number of times I was given the postmark of a silent corner on the stool, with the badge of success in the form of a funny looking hat on my head! In any case, you will find that I have respected your desire to remain unmentioned by name. Surely they would not still be expecting to be paid!

I suppose that VK3 thought that I would not see it, I suppose that VK3 thought that if they could sneak it through very quietly, nobody would utter a protest. Well—"Hawkye Parsons" saw it and definitely registers a protest, and especially as I am an ex-VK3 President, if only for three minutes. Editor indeed—why was I given a chance to vote?—do you see how insidious it becomes—firstly on the magazine committee—then on the editorial side—and finally—and then whom-m-m—EDITOR. I write, more in anger than in sorrow—to think my old Division could do this to me! A vote, and a couple of dipthongs to Pincott 3AF7.

Heard Ken 5IM hooked up with Tim 5TW and they both had a kindred subject in the prevalent cold weather. Tim's suggestion re two pairs of underpants seemed to meet with a chilly reception from Ken—Oh I am a one! Frank 5MZ was another one to be complaining of the cold in his contact with Les 5AAO who managed to throw in a little snow on the subject. Frank 5MZ was out there, he pulled out an ace from up his sleeve in the reply that some snow had fallen on Mount Lofy that afternoon. With true VK5 cunning he did not commit himself as to the quantity, but of course the quality of VK5 snow is not to be denied.

My 5MB this month was honoured by an epistle from VK2, from a gentleman who apparently felt that I was somewhat prejudiced against him. Frank 5MZ. How he must have imagined such a thing is beyond me, but anyway I have written back to him with an explanation as to the state of life in the public, and I feel that we will become friends once again—Perhaps.

Strangely enough, I also received a communication from the same state in which I was taken to task for "playing favourites."

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George 5CV, he of the missing receiver, had yet another intruder the other night, and is fast moving into the "not amused" category. The situation is now reaching the stage when a few land mines, etc., must be installed, and how.

Well—VK4 and VK6 are showing signs of becoming restive again, so perhaps I had better close for this month, although as a matter of fact I am not too sure just how well this new Editor joker can handle a red pencil, and with this in view I have cut out the verbosity, long drawn out to you, for this month. I never fear VK5 will back next month, bigger and better than ever—I hope—How is my palsy-wally Pincott 3AFJ, nothing trivial, I hope!! 73 re 5PS—PanSy to you.

The sudden passing of Les (BUX-504) just as these notes were about to be posted away, came as a shock to all VKS members who knew him personally or had contacted him on the air. His jovial nature and keen interest in Amateur Radio always made his contacts interesting, and it was a pity that he did not reside in the city or suburbs at the same time or as close as would have made an excellent Council member displaying an excellent keenness in the administrative doings of the Division. Les will be missed by all with whom he came in contact.

Institute of Health, North Shore, Auckland, New Zealand.
 Institute of Health, continued to be well attended, and it is pleasing to note the number of visitors to our ranks. Had the pleasure of meeting an old-timer (Ham-wise that is) at a recent meeting. VKSLU in person. Lou told me that after suffering a stroke some time back, he practised "his paralytic" to regain the use of his "paralytic" dis-
 membered hand. Now he is a bona fide come back on the breeze and dish it out with the best of them, probably better than some!

Well, that just about winds it up for now and remember—keep your weather eye open now that PanSy is toting his grease-gun.

TASMANIA

So the R.D. Contest is over again for another year, and although I can't say for sure, I reckon VK7 has won, but then people can be contrary creatures—maybe we could win, it's up to you, each and every one of you, to get that log posted away NOW. Do not procrastinate (that means delay, to save you looking it up). If you post your log then VK7 will win.

The last A.O.C.P. exams saw three Hobart "2" calls (Winston ZAF, Mike ZAV, and Dave ZMD) trying for their c.w. and they appeared very confident, and are more than hopeful. Ian ZZZ seems there should be a further batch of 7 or 8 for the October exam (including me, so he says). Ian is to be commended for the amount of time and effort he has put into the N.C.W. sessions, and at the time of writing is having a spell, before starting 8 nights a week again on 3.035 Mc., commencing on Tuesday, August 16 at 2000 hrs, then every Thursday, Sunday and Tuesday. Between times of course, he has still managed his usual amount of DX, and other divisional work, and yet he always seems to find time to help other Amateurs out, and should by now have his tower up and working.

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"QST"

red TEB has been heard on the air a little more of late, and from what I've heard on the him, too. Our other TEB has promoted himself, or else someone did it for him, and now has a job which entails quite a bit of intrastate travel, so I've no doubt he'll have a s.s.b. mobile in the car before long. Talking of sideband, if TWI isn't using this mode by now, then something is definitely wrong, we plan to be operational on s.s.b. by the 14th August, and you know what that day is, don't you?

At the July Council meeting, your Council had the usual yearly job of "dropping the s.s.b." and regret to say it fell 18 times, and it included some full members—too many full members!

Next year we intend to send everybody an account at the beginning of our financial year, so there will be no excuse for overlooking your sub.

Won't be long now till November, and that's Hamfest month, start thinking about the last week-end of the 11th month, and try to make it this time for both the Saturday night and the Sunday.

Enough for now, see you again next month. 73, VK7ZAS.

HAMADS

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DO YOU KNOW anyone who has built an s.s.b. transistor transceiver, 80, 40, 20 metres using locally available parts? Please! Circuit details required by G. Robinson, 11 Bourke St., Ringwood, Vic. Phone 870-8085.

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Approximate frequency, 200 Mc. Contains 46 miniature tubes, \$30.

★ 3J160E HIGH POWER TRIODES

120 Mc. full ratings. Heater 10v. 29a., anode max. volts 3000v., anode max. current 1000 mA., r.f. output 2150 watts. \$8 each.

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Communication Receivers, Test Equipment, etc. Call, write or phone. Equipment inspected and picked up at your convenience any night or week-end.

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EF50, 20c ea.; 7C7, 10c ea.; CV131, 6CQ6, 50c ea.; 6AC7, 20c ea.; 6AL5, 20c ea.; 6C4, 6AM5, 50c ea.

★ SIGNAL GENERATORS

Type LSG10, 120 Kc. to 260 Mc., \$26. Type LSG11, 120 Kc. to 390 Mc., provision for xtal, \$30, both plus freight.

TE22 Audio Generator, freq. range: sine 20 c.p.s. to 200 kc., square 20 c.p.s. to 25 kc., in four ranges. Output, 7v. p-peak. Output impedance, 1,000 ohms. Price \$42.

★ METERS, P25 TYPE

0-500 uA., \$5.25; 0-100 uA., \$6.95; 0-1 mA., \$4.50; 0-10 mA., \$4.50; 0-50 mA., \$4.50. Full range of Meters and Multi-Testers available.

★ CO-AXIAL CABLE

UR70 72 ohms, 3/16 inch diam., in 27-yard rolls, \$2 plus 75c pack and post. In as-new condition.

★ RAIB COMMUNICATIONS RECEIVER

150 Kc. to 15 Mc. in six bands. B.f.o., etc. Genuine original condition, with a.c. power supply, \$70.

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Brand new. OC72, OC44, 2N132, OC66, OC45, 80c each. AT1138 Power Transistor, 30w., Class B, \$3. Also Diodes: OA71, OA81, OA95, 35c each.

★ SR700A TRIPLE CONVERSION COM. RECEIVER

80 metres to 10 metres. 1st and 3rd oscillators xtal controlled, 3.4-4.0 Mc. tunable i.f., selectable sidebands, 85:1 geared dial, v.f.o. output for transceive operation, selectivity: 0.5, 1.2, 2.5, 4 kc. Internal 1 Mc. xtal calibrator (xtal supplied). Undoubtedly the finest receiver ever to come out of Japan. \$500, 10% discount for cash.

★ MILLER 455 Kc. PRE-WIRED I.F. STRIPS

Comprises two i.f. stages, ceramic filter, diode detector, 55 db. gain, NPN silicon transistors, d.c. requirements 6v. d.c. 2 mA., size 1½ x ½ x ½ inch. \$8.70 inc. tax.

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100,000 ohms per volt. Ranges, d.c. volts: 0.5, 2.5, 10, 50, 250, 500, 1K; a.c. volts: 2.5, 10, 50, 250, 1K; d.c. current: 10 uA., 1 mA., 25 mA., 250 mA., 10 amp; resistance: 20K, 200K ohms, 2 megohms, 20 megohms. To clear, \$25.95.

★ POTENTIOMETERS

Wire wound, 40c each; carbon, 25c each.

★ RESISTORS

½ watt, I.R.C., Welwyn, Eire, Ducon, Philips, \$2 per 100.

★ ½ H.P. 2-STROKE MOTORS

Ohlsson and Rice. Brand new, just imported from America. Weighs only 5½ lbs. 6,300 r.p.m., supplied with 3:1 reduction gearbox, output 2,100 r.p.m. Ideal for driving Alternators for Field Days. Fuel consumption 1 pint per hour. \$30.

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Measurement Ranges:

D.C. V.: 5, 25, 100, 250, 500v (50k ohm/v.);
1000, 5000v. (25k ohm/v.).
A.C. V.: 5, 25, 100, 250, 500, 1000v. (5k ohm/v.).
D.C. A.: 25μA.; 2.5, 25, 250 mA.
OHM: 0 to 10k, 0 to 100k, 0 to 1 MΩ.
0 to 100 MΩ (min. 2 ohm and max. 100 MΩ ohm).
DB.: — 20 to plus 16 to plus 62 db.
Batteries: 1.5v. (UM-2) x 1 and 22.5v. (BL-015) x 1.
Size: 6 1/2 in. x 5 1/2 in. x 3 1/2 in.
Weight: 3.2 lb.

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● Specially designed A.C. current ranges measure up to 10 amperes.
● Germanium diode rectifiers.
● Wide-range and versatile instrument for all-round service and laboratory use. ● Diode protected.

Measurement Ranges:

D.C. V.: 0.5, 2.5, 10, 50, 250, 500, 1000, 5000v
(20k ohm/v.).
A.C. V.: 2.5, 10, 50, 250, 1000v. (4k ohm/v.).
D.C. A.: 50 μA.; 1, 10, 50, 250 mA.; 1, 10 A.
A.C. A.: 250 mA.; 1, 10 A.
OHM: RX1, RX100, RX1000, RX10000 (min. 1 ohm and max. 50 MΩ ohm).
DB.: — 20 to plus 10 db. plus 10 to plus 35 to plus 62 db.
Batteries: 1.5v. (UM-2) x 2 and 22.5v. (BL-015) x 1.
Size: 7 in. x 5 1/2 in. x 3 1/2 in.
Weight: 3.1 lb.

Price: \$34.50 plus S.T. 12 1/2%

MODEL 380-C

● High-grade circuit tester of 30-microampere sensitivity. ● Ruggedly constructed to withstand the wear and tear of heavy-duty service.
● Large mirrored scale dial for accurate reading.

Measurement Ranges:

D.C. V.: 0.5, 3, 12, 60, 300v. (33.3k ohm/v.),
1200, 3000 v. (16.6k ohm/v.).
A.C. V.: 3, 12, 30, 120, 300, 1200v. (5k ohm/v.).
D.C. A.: 30 μA.; 3, 30, 300 mA.
OHM: X1, X10, X100, X1000 (min. 0.5 ohm and max. 20 MΩ ohm).
DB.: — 20 to plus 10 to plus 23 db. up to plus 63 db.
μF (C): 0.001 to 100 μF.
μF (L): 0.1 to 2000 μF.
Batteries: 1.5v. (UM-2) x 4 and 1.5v. (UM-2) x 1.
Size: 7 1/2 in. x 5 in. x 4 in.
Weight: 2.5 lb.

Price: \$23.50 plus S.T. 12 1/2%

MODEL U-50

● Handy meter of 35-microampere sensitivity.

Measurement Ranges:

D.C. V.: 0.1, 0.5, 5, 50, 250, 1000v. (20k ohm/v.).
A.C. V.: 2.5, 10, 50, 250, 1000v. (8k ohm/v.).
D.C. A.: 50 μA.; 0.5, 5, 50, 250 mA.
OHM: RX1, RX10, RX100, RX1k (min. 1 ohm and max. 3 MΩ ohm).
DB.: — 20 to plus 62 db.
μF (C): 100 pF. to 0.2 μF.
Megohm: 1 to 500 MΩ ohm.
Batteries: 1.5 v. (UM-3) x 2.
Size: 5 1/2 in. x 3 1/2 in. x 1 1/2 in.
Weight: 13.3 oz.

Price: \$13.50 plus S.T. 12 1/2%

MODEL 370-X

● Multi-purpose tester covering practically all measuring requirements. ● Two current ranges afford the meter a dual function as a circuit tester and A.C.-D.C. ammeter.

Measurement Ranges:

D.C. V.: 3, 6, 12, 120, 300, 1200, 3000v. (4k ohm/v.).
A.C. V.: 6, 12, 120, 300, 1200, 3000v. (4k ohm/v.).
D.C. A.: 0.3, 3, 30, 300 mA.; 3, 12 A.
A.C. A.: 0.3, 3, 30, 300 mA.; 3, 12 A.
OHM: R, 10R, 100R, 1000R (min. 2 ohm and max. 10 MΩ ohm).
DB.: — 10 to plus 17 db., 0 to plus 23 to plus 62 db.
Batteries: 1.5v. (UM-2) x 2 and 22.5v. (BL-015) x 1.
Size: 6 1/2 in. x 5 1/2 in. x 3 1/2 in.
Weight: 2.6 lb.

Price: \$20.50 plus S.T. 12 1/2%

MODEL P-1B

● Rugged and accurate midjet tester. ● Miniature to the limit of practical use. ● Useful to check all sorts of electrical home appliances.

Measurement Ranges:

D.C. V.: 10, 50, 250, 1000v. (1k ohm/v.).
A.C. V.: 10, 50, 250, 1000v. (1k ohm/v.).
D.C. A.: 100 mA.
OHM: 0.1, 100k ohm (mid-scale — 25k ohm).
DB.: — 10 to plus 22 db. plus 20 to plus 36 db.
μF & H: 0.001 to 0.1 μF, and 10 to 1000H.
Battery: 1.5v. (UM-3) x 1.
Size: 4 1/2 in. x 2 1/2 in. x 1 1/2 in.
Weight: 9 oz.

* Use external power.

Price: \$6.25 plus S.T. 12 1/2%

MODEL F-7TR

● The unique range selector is really epoch-making, a red ball appearing in the slot on a clear acrylic dial. ● Half in size compared with conventional testers. ● The meter self-checks the internal batteries.

Measurement Ranges:

D.C. V.: 0.25, 2.5, 10, 50, 250, 1000v. (20k ohm/v.).
A.C. V.: 2.5, 10, 50, 250, 1000v. (8k ohm/v.).
D.C. A.: 50 μA.; 0.5, 5, 50, 250 mA.
OHM: RX1, RX10, RX100, 500k (min. 1 ohm and max. 500 MΩ ohm).
DB.: — 10 to plus 36 db.
L.L.: 20, 2, 0.2 mA.
Batteries: 1.5v. (UM-3) x 1 and 22.5v. (BL-015) x 1.
Size: 3 1/2 in. x 3 1/2 in. x 1 1/2 in.
Weight: 14.4 oz.

Price: \$22.50 plus S.T. 12 1/2%



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